

## Electricity and Magnetism

Electrostatic Unit (ESU) of charge is so chosen that force between  $Q_1$  and  $Q_2$  at distance  $r$  can be  $Q_1 Q_2 / r^2$  dyes. Unit magnetic pole is chosen to make force in  $m_1 m_2 / r^2$ . Field  $E$  such that force is  $EQ$  dynes.

ESU unit of current = no. of ESU of charge / second.

$$\text{div } E \equiv 4\pi\rho \quad \text{all in ESU.}$$

$$\text{Potential } V. \quad E = - \text{grad } V.$$

Magnetic particle. Poles in air distance  $ds$ . Moment =  $m ds = \mu$ .

$$\text{Potential due to magnetic particle} \quad \frac{1}{r} = \mu \cos \theta / r^2 \quad \begin{array}{c} \theta \\ \text{--- cm} \end{array}$$

Magnetic shell of strength  $\phi$ : any element  $dS$  has effect of magnetic particle of moment  $\phi dS$ .

If  $\phi$  is constant, potential is  $-\phi \Omega$ , where  $\Omega$  is solid angle subtended by shell at point in question.

$B$  magnetic induction.  $H$  magnetic force.

$$\iint \underline{B} d\underline{S} = 0 \quad \text{so} \quad \text{div } B = 0.$$

Hence, there exists vector potential  $\underline{A}$  in  $B = \text{curl } \underline{A}$ .

EMU (p 425)  $\rightarrow$  A small current loop produces effect of magnetic particle.

For E.M.V. of current, a current  $i$  flowing in a loop produces magnetic field equal to that of magnetic shell, of strength  $i$ , bounded by loop.

Consequence of this: work done by unit pole in threading current  $i$  is  $4\pi i$ .

$$It \text{ can be deduced that field is } \int \frac{i ds \times \underline{r}}{r^2}$$

$$= \int \frac{i \sin \theta ds}{r^2} \quad ds \perp \theta \quad \text{H}$$

Induced currents. Induced EMF =  $-\frac{dN}{dt} = -\frac{d}{dt}$  flux  $B$ .

$$\int E ds = -\frac{d}{dt} \iint \underline{B} d\underline{S} \quad \therefore \text{curr } E = -\frac{dB}{dt}.$$

The EMF is the work done on unit charge as it goes round circuit. ~~in~~ pp 452-453 Jeeves derive this by considering magnetic field produced by circuit. So current  $i$  is EMV.

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$$p576 \quad -\frac{1}{c} \frac{dH}{dt} = \text{curl } E \quad (S28)$$

$$4\pi j + \frac{1}{c} \frac{\partial E}{\partial t} = \text{curl } H \quad (S29)$$

$j$ ,  $H$ ,  $B$  on EMU.  
 $E$  on ESU.

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Jeans p. 559.

Volume density  $\rho$  at  $x, y, z$  with velocity  $U, V, W$

Thus  $(u, v, w) = (\rho U, \rho V, \rho W)$  in E&S

In eqn (528),  $u, v, w$  in EMU, so  $(\frac{\rho U}{c}, \frac{\rho V}{c}, \frac{\rho W}{c})$  EMU

Thus  $\frac{4\pi}{c}(\rho U + \frac{df}{dt}) = \frac{\partial r}{\partial t} - \frac{\partial f}{\partial z}$  etc

$$\frac{4\pi\rho U}{c} + \frac{1}{c} \frac{dE}{dt} = \text{curl } H$$

$$(\text{Eqn of continuity}) \frac{\partial}{\partial x}(\rho U) + \frac{\partial}{\partial y}(\rho V) + \frac{\partial}{\partial z}(\rho W) + \frac{dc}{dt} = 0$$

$$H = \alpha, \beta, \gamma \quad B = a, b, c \quad \delta 432 \quad E = (X, Y, Z)$$

$$\text{Inductance} = N = \iint B \cdot dS$$

$$\text{Potential in circuit} = \oint E \cdot ds = \iint \frac{dB}{dt} \cdot dS$$

$$\iint \text{curl } E \cdot dS = - \iint \frac{dB}{dt} \cdot dS$$

$$\therefore - \frac{dB}{dt} = \text{curl } E$$

$$- \frac{dH}{dt} = \text{curl } E \quad \text{all in EMU} \quad \text{p 571}$$

$$H = \text{curl } A \quad \text{curl}(E + \frac{dA}{dt}) = 0$$

$$\therefore E = - \frac{dA}{dt} \neq -\text{grad } \phi$$

$$\text{curl } H = 4\pi j$$

Transition to basic concepts of vector- and tensor-algebra.

Discusses concepts, in 3 and 4 dimensions, that are available to physicists from viewpoint of invariance.

1.  $n=3$  ( $x, y, z$ ) Restrict group to homog. orthogonal.

(10)  $x^2 + y^2 + z^2$  is simplest invariant. Plus form

(11)  $x'x + y'y + z'z$  Dot product

(11) being invariant,  $x'y'z'$  is both co-predicat and contrapredicat to  $xyz$ . For ortho. Transformations the distinction disappears

(12)  $\begin{vmatrix} x & y & z \\ x' & y' & z' \\ x'' & y'' & z'' \end{vmatrix}$ . Transformation multipl by +1 or -1.

Its determinant =  $x(y'z'' - y''z') + y(z'x'' - z''x') + z(x'y'' - x''y')$

(13)  $y'z'' - y''z', z'x'' - z''x', x'y'' - x''y'$

is contrapredicat to  $x, y, z$ . Vector product.

(14)  $ax^2 + by^2 + cz^2 + 2dxy + 2exz + 2fyz$

Von St. calls  $a, b, c, d, e, f$  def a Tensor. For affine trans.  
these may differ in rank: for real coefficients, in  
Trägheitsindex. If we restrict ourselves to ortho. Trans.  
 $x^2 + y^2 + z^2$  is invariant, and this leads us to consider

(15)  $\begin{vmatrix} a & b & c \\ f & b+c & d \\ e & d & c+b \end{vmatrix}$  The cofactor on the

3 fundamental orthogonal invariant of the tensor.

(16)  $\lambda^2 + \lambda^2(a+b+c) + \lambda(b+c+a+ab+cd-e^2-f^2) + \begin{vmatrix} a & f & e \\ f & b & d \\ e & d & c \end{vmatrix}$

We can form from them invariant

(17)  $(a+b+c)^2 - 2(b+c+a+d^2-e^2-f^2) = a^2 + b^2 + c^2 + 2d^2 + 2e^2 + 2f^2$

Formerly the polar (18)  $aa' + bb' + cc' + 2dd' + 2ee' + 2ff'$   
we see that  $a, b, c, d\sqrt{2}, e\sqrt{2}, f\sqrt{2}$  are contrapredicats to  
themselves. From (16) we see they are contrapredicats to

(18')  $x^2, y^2, z^2, yz\sqrt{2}, zx\sqrt{2}, xy\sqrt{2}$

Hence co-predicat to them.

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E.S. unit of charge. Force =  $Q_1 Q_2 / r^2$  in vacuum.  
This defines unit.

E.M. unit of magnetic pole Force =  $m_1 m_2 \mu r^2$  in vacuum.  
E.M. unit of current.

In unit magnetic field, experiences 1 dyne on each centimetre.

Unit of electricity is that produced by unit current in unit time. EM units carry dashes.

$$c = i/i' = Q/Q'$$

(a) Current  $i'$ , length  $ds$  produces  $i' ds \sin \theta$  at distance  $r$ .

(b) By integration, infinite straight wire produces

$$H = 2i'/a \text{ or distance } a.$$

(c) Magnetic pole of strength  $m$ , at distance  $a$ , experiences force  $2mi/a$ . Carried round wire, work done =  $4\pi i' m$ . Independent of path.

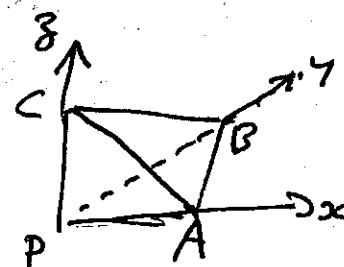
Let circulation/area have components  $X_c, Y_c, Z_c$  near P.

$$\text{circ } BCP = X_c b S$$

$$\text{circ } CAP = Y_c m S$$

$\text{circ } ABP = Z_c n S$  where  $S$  is area of ABC  
since projections of ABC have areas  $bS, mS, nS$ .

$$\frac{\text{circ } ABC}{\text{area } ABC} = lX_c + mY_c + nZ_c$$



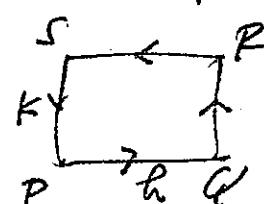
Thus circulation per unit area for infinitesimal density components of  $(X, Y, Z)$  along normal.

Now let  $(X, Y, Z)$  be force of which we are finding circulation per unit area

$$= (X_{QR} - X_{PS}) k + (Y_{PC} - Y_{SR}) h$$

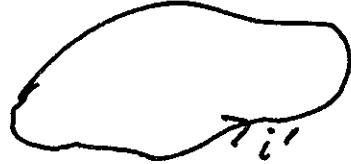
$$= kh \frac{\partial X}{\partial x} - hk \frac{\partial X}{\partial y}$$

$$= kh \left( \frac{\partial Y}{\partial x} - \frac{\partial X}{\partial y} \right) \quad \text{Thus } Z_c = \frac{\partial Y}{\partial x} - \frac{\partial X}{\partial y}$$



Jeans. pp 426-427

A current flowing in a loop has an equivalent magnetic shell.



An element  $dS$  behaves like a magnet of moment  $\phi dS$ ,  $\phi$  being strength of shell.  
If we use E.M.V.,  $\phi = i'$ .

Potential  $\Omega_Q = \iiint \phi d\omega = \phi \omega$   $\omega$  = solid angle.

Work done in carrying unit magnetic pole around a current  $i'$  is  $4\pi i'^2$ . (E.M.V.)

For  $u, v, w$  current in E.M.V.

Displacement current  $\frac{df}{dt}, \frac{ds}{dr}, \frac{dh}{dt}$  in E.S.U. \*

In EMV displacement current is  $\frac{1}{c} \frac{df}{dt}, \frac{1}{c} \frac{ds}{dr}, \frac{1}{c} \frac{dh}{dt}$

Total current in E.M.V. is  $u + \frac{1}{c} \frac{df}{dt}, v + \frac{1}{c} \frac{ds}{dr}, w + \frac{1}{c} \frac{dh}{dt}$

Total current is like incompressible fluid.

Work done in carrying unit magnetic pole around a circuit is  $4\pi$  (Total current through it)

Thus  $4\pi \iint (u + \frac{1}{c} \frac{df}{dt}, \dots) dS = \int H ds$

$$\therefore 4\pi (ij + \frac{1}{c} \frac{df}{dt}), \dots = \text{curl } H$$

In empty space  $u=0$ .

$$(f \mathbf{g}, \mathbf{h}) = \frac{1}{4\pi} \mathbf{E}$$

$$\therefore \text{curl } H = \frac{1}{c} \frac{\partial \mathbf{E}}{\partial t}$$

~~excepting in E.M.V.~~  $H$  in E.M.V.  
 $E$  in E.S.U. (see \* above)

In conducting material,  $(u, v, w) = j$  in E.S.U.

Maxwell's Equations and Tensor  $K_{ij}$ .

$(\frac{Ev_x}{c}, \frac{Ev_y}{c}, \frac{Ev_z}{c}, \rho)$  is a 4-vector for

$$\xi_1 = x, \xi_2 = y, \xi_3 = z, \xi_4 = ct.$$

If we put  $x_1 = \xi_1, x_2 = \xi_2, x_3 = \xi_3, x_4 = i\xi_4$  we must transform the vector in the same way as we have done the coordinates. The vector becomes  $(\frac{Ev_x}{c}, \frac{Ev_y}{c}, \frac{Ev_z}{c}, i\rho)$ .

As  $\square A = \frac{-4\pi\rho}{c}$ ,  $\square V = -4\pi\rho$  we must write

$(A_1, A_2, A_3, iV)$  for the potential 4-vector.

It is contravariant. (We arrived at  $Ev_x/c$  etc. by considering  $dx^1, dx^2, dx^3, dx^4$ ) However, in orthogonal system the distinction disappears, so we may write it as covariant

$$dt, s_1 = dt, s_2 = dx_2, s_3 = dx_3, s_4 = iV.$$

$$\text{Let } K_{ij} = \frac{\partial s_i}{\partial x_j} - \frac{\partial s_j}{\partial x_i}$$

$$K_{12} = \frac{\partial s_1}{\partial x^2} - \frac{\partial s_2}{\partial x^1} = \frac{\partial dt}{\partial x^2} - \frac{\partial dx_2}{\partial x^1} = -H_3.$$

$$K_{13} = \frac{\partial s_1}{\partial x^3} - \frac{\partial s_3}{\partial x^1} = \frac{\partial dt}{\partial x^3} - \frac{\partial dx_3}{\partial x^1} = H_2$$

$$K_{14} = \frac{\partial s_1}{\partial x^4} - \frac{\partial s_4}{\partial x^1} = \frac{\partial dt}{\partial x^4} - \frac{\partial iV}{\partial x^1} = i\left[-\frac{1}{c}\frac{\partial dt}{\partial t} - \frac{\partial V}{\partial x}\right]$$

$$= iE_1 = \xi_1. \quad \text{for } E = -\frac{1}{c}\frac{\partial A}{\partial t} - \nabla V.$$

$$K_{23} = \frac{\partial s_2}{\partial x^3} - \frac{\partial s_3}{\partial x^2} = \frac{\partial dx_2}{\partial x^3} - \frac{\partial dx_3}{\partial x^2} = -H_1, \quad (\text{eqn 1, NS7})$$

$$K_{24} = \frac{\partial s_2}{\partial x^4} - \frac{\partial s_4}{\partial x^2} = \frac{\partial dx_2}{\partial x^4} - \frac{\partial iV}{\partial x^2} = i\left(-\frac{1}{c}\frac{\partial A_2}{\partial t} - \frac{\partial V}{\partial x}\right) = iE_2 = \xi_2$$

$$K_{34} = \frac{\partial s_3}{\partial x^4} - \frac{\partial s_4}{\partial x^3} = \frac{\partial dx_3}{\partial x^4} - \frac{\partial iV}{\partial x^3} = i\left(-\frac{1}{c}\frac{\partial A_3}{\partial t} - \frac{\partial V}{\partial x}\right) = iE_3 = \xi_3$$

$$\therefore K = \begin{pmatrix} 0 & -H_3 & H_2 & \xi_1 \\ H_3 & 0 & -H_1 & \xi_2 \\ -H_2 & H_1 & 0 & \xi_3 \\ -\xi_1 & -\xi_2 & -\xi_3 & 0 \end{pmatrix}$$

In these symbols the Maxwell eqns are

$$0 = \cdot + \frac{\partial K_{12}}{\partial x_2} + \frac{\partial K_{13}}{\partial x_3} + \frac{\partial K_{14}}{\partial x_4}$$

$$0 = \frac{\partial K_{21}}{\partial x_1} + \frac{\partial K_{23}}{\partial x_3} + \frac{\partial K_{24}}{\partial x_4}$$

$$0 = \frac{\partial K_{31}}{\partial x_1} \quad \frac{\partial K_{32}}{\partial x_2} \quad \cdot \quad \frac{\partial K_{34}}{\partial x_4}$$

$$0 = \frac{\partial K_{41}}{\partial x_1} + \frac{\partial K_{42}}{\partial x_2} + \frac{\partial K_{43}}{\partial x_3} \quad \cdot$$

$$0 = \frac{\partial K_{ij}}{\partial x^j}$$

This is a tensor equation, that is accordingly valid in any system.

$$K_{ij} = \frac{\partial s_i}{\partial x_j} - \frac{\partial s_j}{\partial x_i}$$

$$\frac{\partial K_{ij}}{\partial x^k} = \frac{\partial^2 s_i}{\partial x^j \partial x^k} - \frac{\partial^2 s_j}{\partial x^k \partial x^i}$$

The second term is obtained from the first by cyclic permutation,  $(ijk)$

$$\text{Here } \frac{\partial K_{ij}}{\partial x^k} + \frac{\partial K_{jk}}{\partial x^i} + \frac{\partial K_{ki}}{\partial x^j} = 0.$$

If two of  $i, j, k$  are equal, say  $i=j$ , LHS becomes

$$0 + \frac{\partial K_{ik}}{\partial x^i} + \frac{\partial K_{ki}}{\partial x^i} = \frac{\partial}{\partial x^i} (K_{ik} + K_{ki}) = \frac{\partial}{\partial x^i} 0.$$

We get substantial results only when  $i, j, k$  distinct. There are 6 ways of choosing 3 distinct left numbers from 1, 2, 3, 4.

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i=2 j=3 k=4.

$$\frac{\partial K_{23}}{\partial x^4} + \frac{\partial K_{34}}{\partial x^2} + \frac{\partial K_{42}}{\partial x^3} = -\frac{\partial H_1}{\partial x^4} + \frac{\partial \xi_3}{\partial x^2} - \frac{\partial \xi_2}{\partial x^3} \quad II(1)$$

i=1 j=3 k=4

$$\frac{\partial K_{13}}{\partial x^4} + \frac{\partial K_{34}}{\partial x^1} + \frac{\partial K_{41}}{\partial x^3} = \frac{\partial H_2}{\partial x^4} + \frac{\partial \xi_3}{\partial x^1} - \frac{\partial \xi_1}{\partial x^3} \quad II(2)$$

i=1 j=2 k=4

$$\frac{\partial K_{12}}{\partial x^4} + \frac{\partial K_{24}}{\partial x^1} + \frac{\partial K_{41}}{\partial x^2} = -\frac{\partial H_3}{\partial x^4} + \frac{\partial \xi_2}{\partial x^1} - \frac{\partial \xi_1}{\partial x^2} \quad II(3)$$

i=1 j=2 k=3

$$\frac{\partial K_{12}}{\partial x^3} + \frac{\partial K_{23}}{\partial x^1} + \frac{\partial K_{31}}{\partial x^2} = -\frac{\partial H_3}{\partial x^3} - \frac{\partial H_1}{\partial x^1} - \frac{\partial H_2}{\partial x^2} \quad II(4).$$

## Velocities of molecules in a gas.

Assumption of molecular chaos. Randomness. In particular, no direction singled out.

Let velocity  $V$  have components  $x, y, z$ . If the probability of first component being in  $x, x+dx$  is  $f(x)dx$ , the probability for  $y$  must be given by  $f(y)dy$  and for  $z$ ,  $f(z)dz$ .

Thus probability of ~~velocity~~ velocity lying near  $(x, y, z)$  within a region of volume  $dxdydz$  is  $f(x)f(y)f(z)dxdydz$ .

For any small region, we have  $f(x)f(y)f(z)dV$ , where  $dV$  is its volume.

If no direction is singled out, the probability of a speed  $v$  should be the same for all directions - that is to say, it should depend only on the magnitude of  $v$ . Now  $v^2 = x^2 + y^2 + z^2$ . Thus we should have  $f(x)f(y)f(z) = \varphi(x^2 + y^2 + z^2) = \varphi(v^2)$

$$\frac{\partial}{\partial x} : f'(x) f(y) f(z) = \varphi'(x^2 + y^2 + z^2) \cdot 2x.$$

$$\text{Divide } \frac{f'(x)}{f(x)} = \frac{2x \varphi'(v^2)}{\varphi(v^2)}$$

$$\therefore \frac{1}{2x} \frac{f'(x)}{f(x)} = \frac{\varphi'(v^2)}{\varphi(v^2)}$$

Hence each side is constant.

$$\frac{1}{2x} \frac{f'(x)}{f(x)} = c$$

$$\frac{f'(x)}{f(x)} = 2cx$$

$$\ln f(x) = cx^2$$

$$\therefore f(x) = e^{cx^2}$$

If  $c > 0$ , we have large probabilities for large velocities.

Put  $c = -a$ .

$$f(x) = e^{-ax^2}$$

$$f(x)f(y)f(z) = e^{-a(x^2 + y^2 + z^2)} = e^{-av^2}$$

For lie between if the velocity lies between  $v$  and  $v+dv$ , the end of the velocity vector must lie in a region of volume  $4\pi v^2 dv$ . The probability of this is  $4\pi v^2 e^{-av^2} dv$ .

Graph



PROBLEMS RELATED TO ORTHOGONAL MATRICES.

1. Write the matrix  $M$  for rotation through  $\theta$ . What is the geometrical meaning of  $M^T$ ? Is there any operation, other than transposition, that will change  $M$  to  $M^T$ ? Of what general theorem is this an example?

Find the eigenvalues of  $M$ , and plot them on the Argand Diagram. Why might these values be expected?

2. Find the matrix  $M$  for the rotation that sends  $OX$  to  $OY$ ,  $OY$  to  $OZ$ , and  $OZ$  to  $OX$ . Find  $M^2$  and  $M^3$ .

$M$  has only one real eigenvector; call it  $v$ . Find  $v$  and the eigenvalue associated with it.

Choose new axes, which are not to involve any change of scale on the axes. The first axis is to be in the direction of  $v$ ; the other two are to be perpendicular to  $v$  and to each other. Let  $X, Y, Z$  be co-ordinates in this new system. Find the matrix  $L$  that gives  $x, y, z$  in terms of  $X, Y, Z$ ; find the matrix  $N$  that gives  $X, Y, Z$  in terms of  $x, y, z$ . Mention anything you notice when comparing  $L$  and  $N$ , and explain it.

3. Choose any 3 perpendicular unit vectors,  $u, v, w$ . Do not take obvious ones; none of them should be along any original axis.  $X, Y, Z$  are co-ordinates based on  $u, v, w$ . Write the equations giving  $x, y, z$  in terms of  $X, Y, Z$ ; also the equations giving  $X, Y, Z$  in terms of  $x, y, z$ .

Choose an ellipsoid having axes in the directions of  $u, v, w$ . Write its equation (i) in terms of  $X, Y, Z$ , (ii) in terms of  $x, y, z$ . Write the matrix associated with its equation in the  $x, y, z$  system. Find its eigenvalues and eigenvectors. Comment on the result.

1. Find the shape and orientation of the conic  $36x^2 + 24xy + 29y^2 = 180$ . (Find the eigenvalues of the associated matrix and take co-ordinate axes along them.)

2. Find the 10th power of the matrix  $\begin{pmatrix} 5/2 & -1/2 \\ -1/2 & 5/2 \end{pmatrix}$ .

What is the most complicated fraction that can occur in the  $n^{th}$  power of this matrix?

Exercise. The transformation  $S = \begin{pmatrix} 2 & 3 \\ 1 & 2 \end{pmatrix}$   
 and the matrix  $M = \begin{pmatrix} 10 & -6 \\ 2 & 3 \end{pmatrix}$ .

Q2

Find the matrices, as shown in the new axes, for the transformation and for the conic defined by  $\mathbf{v}^T M \mathbf{v} = \text{constant}$ .

Solution.  $S = \begin{pmatrix} 2 & 3 \\ 1 & 2 \end{pmatrix}$  has the inverse  $\begin{pmatrix} 2 & -3 \\ -1 & 2 \end{pmatrix} = S^{-1}$ .

$M$  as a transformation appears at  $S^{-1}MS$  in

the new axes.  $\begin{pmatrix} 2 & -3 \\ -1 & 2 \end{pmatrix} \begin{pmatrix} 10 & -6 \\ 2 & 3 \end{pmatrix} \begin{pmatrix} 2 & 3 \\ 1 & 2 \end{pmatrix} = \begin{pmatrix} 14 & -21 \\ -6 & 12 \end{pmatrix} \begin{pmatrix} 2 & 3 \\ 1 & 2 \end{pmatrix}$

$$= \begin{pmatrix} 7 & 0 \\ 0 & 6 \end{pmatrix}.$$

$$\text{For a conic } S^T M S = \begin{pmatrix} 2 & 1 \\ 3 & 2 \end{pmatrix} \begin{pmatrix} 10 & -6 \\ 2 & 3 \end{pmatrix} \begin{pmatrix} 2 & 3 \\ 1 & 2 \end{pmatrix}$$

$$= \begin{pmatrix} 22 & -9 \\ 34 & -12 \end{pmatrix} \begin{pmatrix} 2 & 3 \\ 1 & 2 \end{pmatrix} = \begin{pmatrix} 35 & 48 \\ 86 & 78 \end{pmatrix}$$

## MATRICES.

The matrix  $\begin{pmatrix} a & b \\ c & d \end{pmatrix}$  can arise as an abbreviation for the transformation  $(x, y) \rightarrow (x^*, y^*)$  where  
(I)  $x^* = ax + by$ , (II)  $y^* = cx + dy$ .  $Mv$  for short.

This is probably the most natural way into the subject of matrices.

A matrix can also be used to specify the expression  $ax^2 + 2hxy + by^2$  as  $(x \ y) \begin{pmatrix} a & h \\ h & b \end{pmatrix} (x \ y)$ .

To do this we have to bring in the row vector  $(x \ y)$  as well as the column vector  $(x)$ .  $(x \ y)$  is known as the transpose of  $(x)$ . We can write  $(x \ y) = (x)^T$ .

Equally, the column vector is the transpose of the row vector. Transposition means that rows are changed to columns and columns to rows. This operation can be applied to a matrix as well as to a vector.

The expression (II) has the form  $v^T M v$ .

These expressions have geometrical significance.  $v^T M v = \text{constant}$  is the equation of a conic. If P is a point on this conic, and  $v = OP$  it can be proved that  $Mv$  is a vector giving the direction of the normal to the conic at P.

## Transpose of a product.

The product  $A=BC$  is given by the formula  $a_{ik} = \sum b_{ij} c_{jk}$ . The transpose of A,  $a^T$  has  $a^T_{ik} = a_{ki} = \sum b_{kj} c_{ji}$ . The formula for a matrix product must have the form  $(\ )_{ik} = \sum (\ )_{ij} (\ )_{jk}$ , which is not so in the equation above. We can bring it

to this form by using  $b_{kj} = b^T_{jk}$  and  $c_{ji} = c^T_{ij}$ . This gives  $a^T_{ik} = \sum b^T_{jk} c^T_{ij} = \sum c^T_{ij} b^T_{jk}$ , which indicates that  $A^T = C^T B^T$ . The transpose of a product is the product of the transposes in the reverse order.

**Exercise.** Consider the case in which  $M = \begin{pmatrix} 10 & -6 \\ 2 & 3 \end{pmatrix}$  and  $S = \begin{pmatrix} 2 & 3 \\ 1 & 2 \end{pmatrix}$ . Find the matrices that correspond to  $M$  in the new axis system (i) when  $M$  is used to define a transformation, (ii) when  $M$  is used to define a conic.

#### Transformations that preserve lengths and angles.

It is an advantage of matrix notation that the theory takes the same form in any number of dimensions. If a rigid body moves, all the lengths and angles are unaltered, so it is natural to consider transformations that have this property. There are some transformations that have this property but cannot be realized by moving the body - reflections in a mirror, for instance. We shall not exclude these from our considerations.

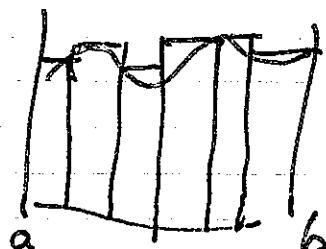
It is possible to find this set of transformations solely from the condition that all lengths are to remain unaltered, for if the lengths of the sides of a triangle are unchanged, the same must be true for the angles in it. However the algebra is slightly simpler if we suppose the condition that all scalar products (dot products) are to remain unaltered. The scalar product,  $u \cdot v$ , can be expressed in matrix notation as  $u^T v$ .

An old joke is that a matrix can represent either an alibi or an alias. "Alibi" means "somewhere else" and can be used to describe a transformation that sends some object to a new position. "Alias" means a new name for the same person, and applies when we change axes, and thus specify the same vectors by a new set of numbers. The algebra is exactly the same in these two cases. You can use either you like to visualize what is happening.

We suppose then that our vectors  $u$  and  $v$  are to be replaced by  $U$  and  $V$ , with  $u=SU$  and  $v=SV$ , and that this is to make no difference when we calculate the scalar product,  $u^T v$ . The transpose rule shows that  $u^T = U^T S^T$ , so  $u^T v$  becomes  $U^T S^T V$ , and we demand that this be the same as  $U^T V$ . Clearly this will be so if  $S^T S = I$ , the identity transformation. In fact this is the only way it can happen.

# Principal Integral P. 1.

Riemann integral is based on diagram



function takes  
finite values,  
 $a, b$  finite

Improper Riemann Integral applies to cases such as

$$\int_1^\infty \frac{1}{x^2} dx \text{ and } \int_0^1 \frac{1}{\sqrt{x}} dx$$

in which  $a, b$  may be infinite, or  $f(x)$  may take infinite value.

(i) Define  $\int_1^\infty \frac{1}{x^2} dx = \lim_{N \rightarrow \infty} \int_1^N \frac{1}{x^2} dx = \left[ -\frac{1}{x} \right]_1^N = -\frac{1}{N} + 1 \rightarrow 1$  as  $N \rightarrow \infty$ .

So  $\int_0^\infty \frac{1}{x^2} dx = 1$ .

(ii) Define  $\int_0^1 \frac{1}{\sqrt{x}} dx$  as  $\lim_{a \rightarrow 0} \int_a^1 \frac{1}{\sqrt{x}} dx$

$$= \left[ 2\sqrt{x} \right]_a^1 = 2 - 2\sqrt{a} \rightarrow 2$$

so  $\int_0^1 \frac{1}{\sqrt{x}} dx = 2$ .

If we try to deal with  $\int_1^b \frac{1}{x} dx$  as

$$\lim_{a \rightarrow 0} \lim_{b \rightarrow \infty} \int_a^b \frac{1}{x} dx + \lim_{b \rightarrow \infty} \int_b^1 \frac{1}{x} dx \quad a, b \text{ finite}$$

We get  $= \lim_{a \rightarrow 0} \left[ \ln(-x) \right]_{-1}^a + \left[ \ln x \right]_b^1$

$$\ln a - 0 + 0 - \ln b = \ln \frac{a}{b}$$

This does not have a definite limit. It depends on the way in which  $a$  and  $b$  tend to zero.

Cauchy was led to define "Principal Integral" for such a situation by work on complex variable.

P.2

(P2)

## The idea of principal integral.

In work on complex variable  $z = x + iy$ ,  
 $w = f(z)$ , we often have to use

$$\int_C f(z) dz \quad \text{the path } C.$$

This has the property that, in a region where  $f(z)$  is well behaved (i.e. analytic),

we may vary the path, provided we keep its end points fixed.

$$\int_a^b f(z) dz \quad \text{if } f$$

Suppose  $f(z)$  has a singularity at  $z = a$ .

and we are interested in  $\int_a^b f(z) dz$

We may vary the path to this:-

This is OK as the function is analytic in the region bounded by the two curves.

The integral now consists of 2 parts.

(1) around the semicircle.

$$(2) \int_a^{-\epsilon} + \int_{-\epsilon}^b$$

This leads us to define the principal integral for  $a \rightarrow b$  as  $\lim_{\epsilon \rightarrow 0} \left\{ \int_a^{-\epsilon} f(z) dz + \int_{-\epsilon}^b f(z) dz \right\}$ ?

Usually  $\int_{-1}^{+1} \frac{dx}{x}$  is meaningless. Graph

on account of the  $-\infty, +\infty$  effect.

At problem 2 I was working on involved  
 $\int_0^k \frac{-\ln t dt}{k-t}$ .

Let  $F(k,t) = \frac{-\ln t}{k-t}$ . Computer gives following values

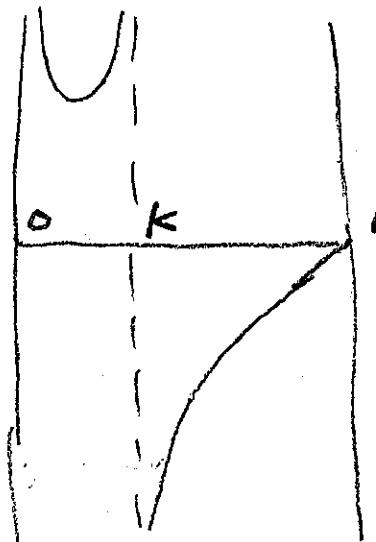
(P3)

Graph of integrand.

$K=C/N$  WITH  $N=20$

$C=?$

$F(0.35, 0.05) = 9.98577425$   
 $F(0.35, 0.1) = 9.21034037$   
 $F(0.35, 0.15) = 9.48559992$   
 $F(0.35, 0.2) = 10.7295861$   
 $F(0.35, 0.25) = 13.8629436$   
 $F(0.35, 0.3) = 24.0794561$   
 $F(0.35, 0.4) = -18.3258146$   
 $F(0.35, 0.45) = -7.98507696$   
 $F(0.35, 0.5) = -4.6209812$   
 $F(0.35, 0.55) = -2.989185$   
 $F(0.35, 0.6) = -2.04330249$   
 $F(0.35, 0.65) = -1.43594305$   
 $F(0.35, 0.7) = -1.01907127$   
 $F(0.35, 0.75) = -0.719205181$   
 $F(0.35, 0.8) = -0.495874558$   
 $F(0.35, 0.85) = -0.325037859$   
 $F(0.35, 0.9) = -0.191564574$   
 $F(0.35, 0.95) = -0.0854888241$   
 $F(0.35, 1) = 0$



The graph near  $t=k$  is approximately symmetric, and the infinity can be made to disappear if we superpose the graph from  $0$  to  $k$ , reversed, on the graph of from  $k$  to  $2k$ . In effect take temporary origin at  $k$  and measure away from  $k$ .

$\int_0^k \frac{-\ln t dt}{k-t} = \int_0^k \frac{-\ln(k-v)}{v} dv + \int_{2k}^{2k} \frac{-\ln(k-v)}{v} dv. \text{ (Consider } k \leq \frac{1}{2}).$

$$\int_0^k \frac{-\ln t dt}{k-t} = \int_{v=k}^{v=0} \frac{-\ln(k-v)}{v} dv = \int_0^k \frac{-\ln(k-v)}{v} dv$$

$$\int_k^{2k} \frac{-\ln t dt}{k-t} = \int_{v=0}^{v=k} \frac{-\ln(k+v) dv}{-v} = \int_0^k \frac{\ln(k+v) dv}{v}$$

P.T. 4

Thus  $\int_0^{2k}$  gives  $\int_0^k \frac{\ln(k+v) - \ln(k-v)}{v} dv$  (P4)

$$\begin{aligned}\ln(k+v) &= \ln k + \ln(1+\frac{v}{k}) \\ \ln(k-v) &= \ln k - \ln(1-\frac{v}{k}) \\ \text{So } \int_0^{2k} &= \int \frac{\ln(1+\frac{v}{k}) - \ln(1-\frac{v}{k})}{v} dv \\ &= \int_0^k \frac{1}{\sqrt{v}} \left\{ \frac{v}{k} - \frac{v^2}{2k^2} + \frac{v^3}{3k^3} - \frac{v^4}{4k^4} \dots \right. \\ &\quad \left. + \frac{v}{k} + \frac{v^2}{2k^2} - \frac{v^3}{2k^3} + \frac{v^4}{4k^4} \dots \right\} dv \\ &= 2 \int_0^k \frac{1}{k} + \frac{v^2}{3k^3} + \frac{v^4}{5k^5} + \dots dv \\ &= 2 \left[ \frac{v}{k} + \frac{v^3}{9k^3} + \frac{v^5}{25k^5} + \dots \right]_0^k \\ &= 2 \left[ 1 + \frac{1}{9} + \frac{1}{25} + \dots \right] \text{ independent of } k! \\ &= 2 \left( \frac{\pi^2}{8} \right) = \frac{\pi^2}{4}.\end{aligned}$$

Independence of  $k$ :  $\int_0^k \frac{\ln(k+v) - \ln(k-v)}{v} dv$

Let  $t = v = ku$ .  $\int_{u=0}^1 \frac{\ln((k+ku) - \ln(k-ku))}{ku} du$

$$= \int_0^1 \frac{\ln(1+w) - \ln(1-w)}{w} dw$$

If  $k=\frac{1}{2}$ ,  $\int_0^{2k} \in \int_0^1$ . We have

Principal  $\int_0^1 \frac{-\ln t}{\frac{1}{2}-t} dt = \frac{\pi^2}{4}$ .

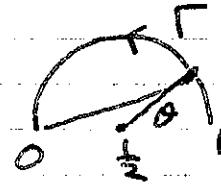
P.I. 5

(P5)

Now principal integral  $\int_0^1 \frac{-\ln t}{t-1} dt$  is the real part of  $\int_0^1 \frac{-\ln t dt}{t-1}$  taken by a path that avoids the singularity  $t=\frac{1}{2}$ . Consider integral along semicircle  $\alpha(0, 1)$ .

Reverse sign of integral, and direction  $0, 1$ .

We get  $\int_{\Gamma} \frac{-\ln t dt}{t-\frac{1}{2}}$ .



At angle  $\theta$  on this semicircle  $t = \frac{1}{2} + \frac{1}{2}e^{i\theta}$

$$\text{so } t - \frac{1}{2} = \frac{1}{2}e^{i\theta}$$

$t$  is at distance  $2(\frac{1}{2} \cos \frac{\theta}{2})$  and angle  $\frac{\theta}{2}$  from origin.

Thus  $t = \cos \frac{\theta}{2} e^{i\theta/2}$   $dt = \frac{1}{2} i e^{i\theta} d\theta$ .

$$dt = \frac{1}{2} \cos \frac{\theta}{2} + i \frac{\theta}{2}$$

$$\therefore \int_{\Gamma} = \int_{\theta=0}^{\pi} \left( -\ln \cos \frac{\theta}{2} - \frac{i\theta}{2} \right) \frac{\frac{1}{2} i e^{i\theta} d\theta}{\frac{1}{2} e^{i\theta}}$$

$$= \int_0^{\pi} \left( -\ln \cos \frac{\theta}{2} - \frac{i\theta}{2} \right) i d\theta$$

$$\text{Real part} = \int_0^{\pi} -\frac{i\theta}{2} d\theta = \int_0^{\pi} \frac{\theta}{2} d\theta$$

$$= \left[ \frac{\theta^2}{4} \right]_0^{\pi} = \frac{\pi^2}{4} \text{ as required.}$$

Woman has some apples. She sells  $\frac{1}{2}$  of her stock and  $\frac{1}{2}$  an apple. Then  $\frac{1}{3}$  of remaining stock and  $\frac{1}{3}$  apple. Then  $\frac{1}{4}$  and  $\frac{1}{4}$  apple. Then  $\frac{1}{5}$  and  $\frac{1}{5}$  apple.

Suppose she begins with  $a$  apples, and has  $b, c, d, e$  at various stages.

$$\text{Step 1} \quad \text{If has } a. \text{ Sells } \frac{1}{2}a + \frac{1}{2} \\ \therefore b = a - \left(\frac{1}{2}a + \frac{1}{2}\right) = \frac{1}{2}a - \frac{1}{2} \\ \therefore a = 2b + 1$$

$$\text{Step 2} \quad \text{If } b \text{ sells } \frac{1}{3}b + \frac{1}{3} \\ \therefore c = b - \left(\frac{1}{3}b + \frac{1}{3}\right) = \frac{2}{3}b - \frac{1}{3}$$

$$\therefore 3c = 2b - 1 \quad \therefore 2b = 3c + 1.$$

$$\text{Step 3} \quad \text{If } c \text{ sells } \frac{1}{4}c + \frac{1}{4} \\ d = c - \left(\frac{1}{4}c + \frac{1}{4}\right) = \frac{3}{4}c - \frac{1}{4}$$

$$\cancel{3c} = 4d = 3c - 1.$$

$$\text{Step 4} \quad \text{If } d \text{ sells } \frac{1}{5}d + \frac{1}{5} \\ e = d - \left(\frac{1}{5}d + \frac{1}{5}\right) \\ = \frac{4}{5}d - \frac{1}{5} \quad \tilde{se} = 4d - 1.$$

Substitution

$$a = 3c + 1$$

$$a = 4d + 1$$

$$a = 5e + 1.$$

$$\therefore a+1 = 3c+3 = 3(c+1)$$

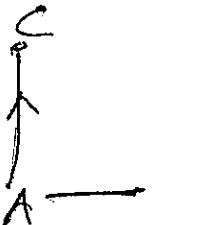
$$a+1 = 4d+4 = 4(d+1)$$

$$a+1 = 5e+5 = 5(e+1)$$

$\therefore a+1$  is divisible by 3, 4, 5.

$$\therefore a = 60k - 1 \quad k \in \mathbb{Z}$$

10 min



Let  $r$  be speed of river  
 $b$ : speed of boat relative to river

Upstream velocity  $b-r$   
 Downstream velocity  $b+r$

$$10 \text{ min} = \frac{1}{6} \text{ hour}$$

 $B \rightarrow$ 

$$\text{so } AC = \frac{1}{6}(b-r)$$

$$BC = 1 + \frac{1}{6}(b-r)$$

Time to row from C to B is

$$\frac{1 + \frac{1}{6}(b-r)}{b+r}$$

Total time from passing upstream thru A is

$$\frac{1}{6} + \frac{1 + \frac{1}{6}(b-r)}{b+r}$$

Time for boat to float from A to B is  $\frac{1}{r}$

$$\frac{1}{r} = \frac{1}{6} + \frac{1 + \frac{1}{6}(b-r)}{b+r}$$

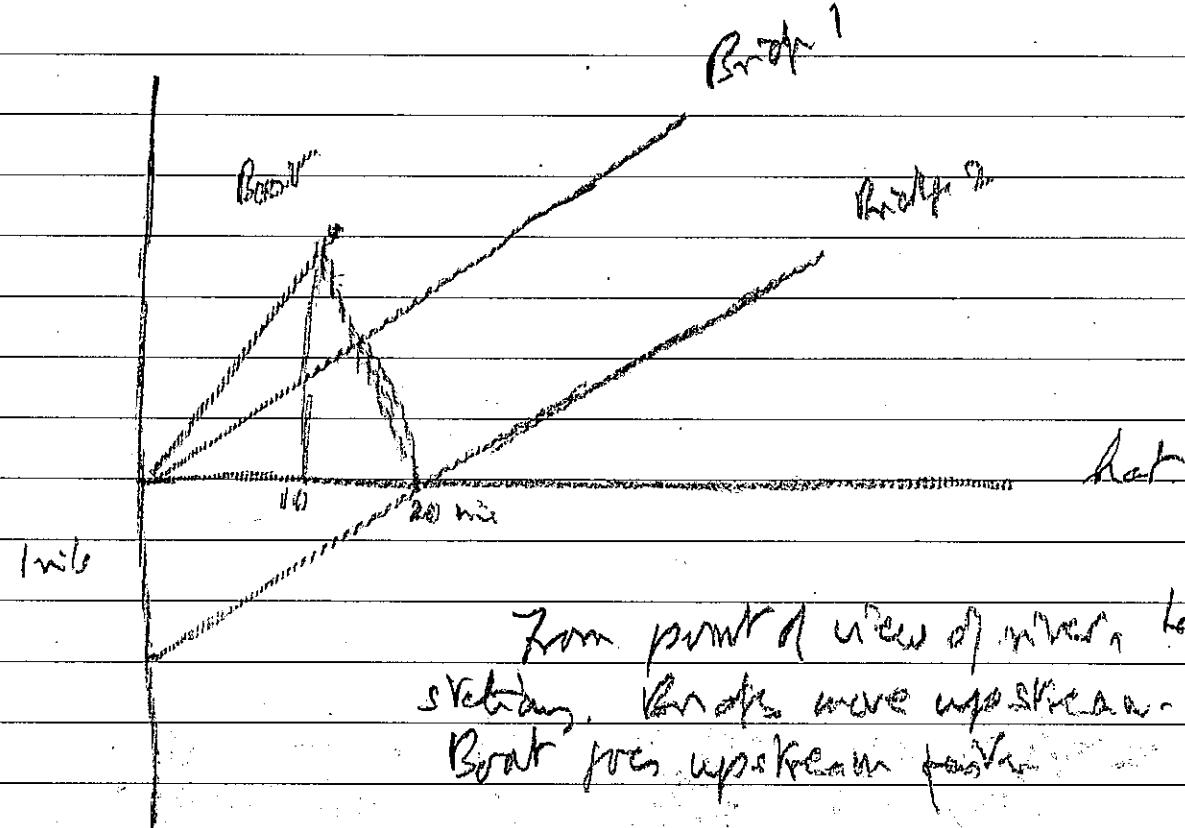
$$x(b+r) : \frac{b+r}{r} = \frac{1}{6}(b+r) + 1 + \frac{1}{6}(b-r)$$

$$= \frac{1}{3}b + 1$$

$$\therefore \frac{b}{r} = \frac{1}{3}b \quad \therefore \frac{1}{r} = \frac{1}{3}$$

$$r = 3$$

P<sub>8</sub>



From point A view of river, boat is  
stationary. Boats move upstream.  
Boat goes upstream faster.

(0.25 0.35)  
0.25 - 0.35

A woman has some apples.  
 She sells  $\frac{1}{2}$  of what she has and  $\frac{1}{2}$  an apple.  
 Then  $\frac{1}{3}$  - - - - -  $\frac{1}{3}$  ..  
 Then  $\frac{1}{6}$  - - - - -  $\frac{1}{6}$  ..  
 Then  $\frac{1}{8}$  - - - - -  $\frac{1}{8}$  apple

Let  $n_0, n_1, n_2, n_3, n_4$  be the number she has after 0, 1, 2, 3, 4 sales.

$$n_1 = n_0 - \left(\frac{1}{2}n_0 + \frac{1}{2}\right) = \frac{1}{2}n_0 - \frac{1}{2} \quad n_0 = 2n_1 + 1 \quad (1)$$

$$n_2 = n_1 - \left(\frac{1}{3}n_1 + \frac{1}{3}\right) = \frac{2}{3}n_1 - \frac{1}{3} \quad 2n_1 = 3n_2 + 1 \quad (2)$$

$$n_3 = n_2 - \left(\frac{1}{4}n_2 + \frac{1}{4}\right) = \frac{3}{4}n_2 - \frac{1}{4} \quad 3n_2 = 4n_3 + 1 \quad (3)$$

$$n_4 = n_3 - \left(\frac{1}{5}n_3 + \frac{1}{5}\right) = \frac{4}{5}n_3 - \frac{1}{5} \quad 4n_3 = 5n_4 + 1 \quad (4)$$

$$n_0 = 2n_1 + 1 \quad (1)$$

$$\text{In (1) substitute for } 2n_1 \text{ from (2)} \quad n_0 = 3n_2 + 2 \quad (2')$$

$$\text{In (2')} \text{ substitute for } 3n_2 \text{ from (3)} \quad n_0 = 4n_3 + 3 \quad (3')$$

$$\text{In (3')} \text{ substitute for } 4n_3 \text{ from (4)} \quad n_0 = 5n_4 + 4 \quad (4')$$

$$\text{Hence } n_0 + 1 = 2(n_1 + 1) \quad \text{from (1)}$$

$$n_0 + 1 = 3(n_2 + 1) \quad \text{from (2')}$$

$$n_0 + 1 = 4(n_3 + 1) \quad \text{from (3')}$$

$$n_0 + 1 = 5(n_4 + 1) \quad \text{from (4')}$$

$\therefore n_0 + 1$  is divisible by 2, 3, 4 and 5

$$\therefore n_0 + 1 = 60k \quad k \in \mathbb{N}.$$

60 is LCM.

If this is so, it will be possible to find  $n_1 + 1, n_2 + 1, n_3 + 1, n_4 + 1$  as whole numbers from last 4 equations, and to deduce from these (1), (2), (3), (4).

$$\text{Then } 60k = 5(n_4 + 1)$$

$$n_4 + 1 = 12k.$$

The simplest solution is  $k=1$ , and 11 apples after all the sales.

P  
/0

### PARTIAL DIFFERENTIATION.

1.) P is the point  $(x,y)$ , Q is  $(X,Y)$ . Find  $OP^2, OQ^2, PQ^2$ .  
What is the condition for  $OP$  to be perpendicular to  $OQ$ ?  
Simplify your result.

If  $\mathbf{u}$  and  $\mathbf{v}$  are the vectors  $(x,y)$  and  $(X,Y)$ , how would  
your result be written in vector notation? What is it  
called?

2. Let  $f(x,y) = (ax^2 + 2hxy + by^2)/2$ . At what rate does  $f(x,y)$   
change if  $(x,y)$  moves with velocity  $(dx/dt, dy/dt)$ ?

If  $a=1, h=0, b=1$ , what is the condition for  $df/dt$  to be  
zero? What does this condition tell you about the vectors  
 $(x,y)$  and  $(dx/dt, dy/dt)$ ? (Remember question 1.) Is this  
reasonable in the light of what you know about geometry?

The line through a point on a curve, perpendicular to the  
tangent is known as the **normal**. If the curve is  
 $f(x,y)=\text{constant}$ , with  $f(x,y)$  as given at the start of this  
question, find a vector that gives the direction of the  
normal to the curve.

P  
II

### PARTIAL DIFFERENTIATION.

1.) P is the point  $(x,y)$ , Q is  $(X,Y)$ . Find  $OP^2, OQ^2, PQ^2$ .  
What is the condition for OP to be perpendicular to OQ?  
Simplify your result.

If  $\mathbf{u}$  and  $\mathbf{v}$  are the vectors  $(x,y)$  and  $(X,Y)$ , how would  
your result be written in vector notation? What is it  
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 $f(x,y)=\text{constant}$ , with  $f(x,y)$  as given at the start of this  
question, find a vector that gives the direction of the  
normal to the curve.

P  
12

### PARTIAL DIFFERENTIATION.

1.) P is the point  $(x, y)$ , Q is  $(X, Y)$ . Find  $OP^2, OQ^2, PQ^2$ .  
What is the condition for  $OP$  to be perpendicular to  $OQ$ ?  
Simplify your result.

If  $\mathbf{u}$  and  $\mathbf{v}$  are the vectors  $(x, y)$  and  $(X, Y)$ , how would  
your result be written in vector notation? What is it  
called?

2. Let  $f(x, y) = (ax^2 + 2hxy + by^2)/2$ . At what rate does  $f(x, y)$   
change if  $(x, y)$  moves with velocity  $(dx/dt, dy/dt)$ ?

If  $a=1$ ,  $h=0$ ,  $b=1$ , what is the condition for  $df/dt$  to be  
zero? What does this condition tell you about the vectors  
 $(x, y)$  and  $(dx/dt, dy/dt)$ ? (Remember question 1.) Is this  
reasonable in the light of what you know about geometry?

The line through a point on a curve, perpendicular to the  
tangent is known as the **normal**. If the curve is  
 $f(x, y) = \text{constant}$ , with  $f(x, y)$  as given at the start of this  
question, find a vector that gives the direction of the  
normal to the curve.

## Xrays Medical Convex

The difference between  $\frac{\partial f}{\partial x}|_y$  and  $\frac{\partial f}{\partial x}|_u$ .

Let  $u = y - x$ .  $f(x, y) = x^2 + y^2$

As  $y = u+x$   $f = x^2 + (u+x)^2$

$$\left(\frac{\partial f}{\partial x}\right)_y = 2x \quad \left(\frac{\partial f}{\partial x}\right)_u = 2x + 2(u+x)$$

P<sub>13</sub>

In a variation of  $(x, y)$  where  $x=t$ ,  $y=c$ .

The point  $(x, y)$  moves along lines  
i.e. along lines  $y=\text{constant}$ .

In a variation where  $u$  is constant

$$y-x=c.$$

If  $x=t$ ,  $y=ct+b$ .

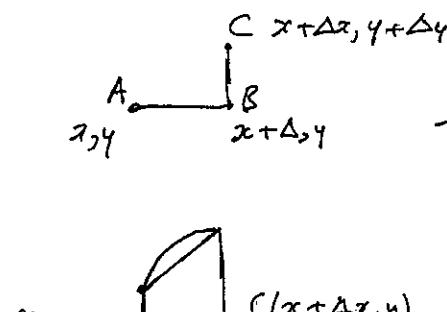
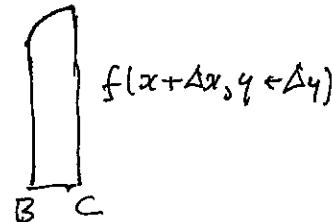
This point  $(x, y)$  moves  
along the lines.



## Partial Differentiation.

Rolle's Theorem

Mean value theorem

There is a point where  $\frac{dy}{dx}$  = gradient of chord. $z = f(x, y)$  given.  $x, y$  grow at rates  $\frac{dx}{dt}, \frac{dy}{dt}$ . What is  $\frac{dz}{dt}$ ?In time  $\Delta t$  (if  $x$  increase by  $\Delta x$ ,  $y$  by  $\Delta y$ ).  
Thus we move from A to C in diagram.

$$f(x, y) = f_A \quad f(x + \Delta x, y) = f_B \quad f(x + \Delta x, y + \Delta y) = f_C$$

In first diagram  $\frac{f_B - f_A}{AB} = \text{gradient at intermediate point} = \frac{\partial f}{\partial x}(x + \alpha \Delta x, y)$ (In second diagram  $\frac{f_C - f_B}{BC} = \frac{\partial f}{\partial y}(x + \Delta x, y + \beta \Delta y)$ )

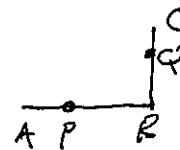
$$\therefore f_C - f_A = (f_C - f_B) + (f_B - f_A) = AB \frac{\partial f}{\partial x}(x + \alpha \Delta x, y) + BC \frac{\partial f}{\partial y}(x + \Delta x, y + \beta \Delta y)$$

 $\frac{dz}{dt}$  is limit of  $\frac{f_C - f_A}{\Delta t}$ , so limit of

$$\frac{\Delta x}{\Delta t} \frac{\partial f}{\partial x}(x + \alpha \Delta x, y) + \frac{\Delta y}{\Delta t} \frac{\partial f}{\partial y}(x + \Delta x, y + \beta \Delta y)$$

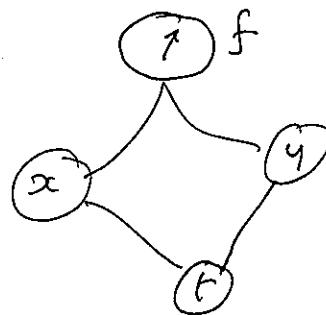
Thus this is related to gradients at P and Q

All we know about P and Q is that they are somewhere on AB and BC.

When  $\Delta t \rightarrow 0$ ,  $\Delta x \rightarrow 0$  and  $\Delta y \rightarrow 0$ . Thus all the points P, B, Q, C tend to A.We have to assume  $\frac{\partial f}{\partial x}$  and  $\frac{\partial f}{\partial y}$  continuous if weare to have  $\frac{dz}{dt} = \frac{\partial f}{\partial x} \frac{dx}{dt} + \frac{\partial f}{\partial y} \frac{dy}{dt}$ .In the counter example  $z = \frac{xy}{r}$ ,  $f(0, 0) = 0$ If we are at a point  $(x, 0)$ ,  $z/r$  is stationary as y coordinate begins to increase, for  $z/r = \cos \theta$ , with max. at  $\theta = 0$ .y grows at rate 1, so  $\frac{\partial f}{\partial y} = 1$  at  $(x, 0)$  where  $x \neq 0$ .So  $z = 0$  for  $x = 0$  and for  $y = 0$ ,  $\frac{\partial f}{\partial x} = 0$  at  $(0, 0)$   $x \rightarrow 0$  does not give this]

- ①  $\frac{df}{dt} = \frac{\partial f}{\partial x} \frac{dx}{dt} + \frac{\partial f}{\partial y} \frac{dy}{dt}$  is often written  
 ②  $df = \frac{\partial f}{\partial x} dx + \frac{\partial f}{\partial y} dy$  and this form is  
 often very convenient.

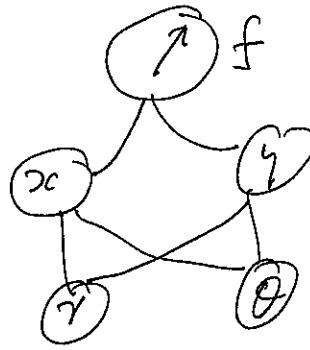
The situation first considered has this scheme. The meter reading,  $f$ , depends on the position of the dials. These dials are driven by a clock,  $t$ .



The equation (2) corresponds to the fact that small changes in  $f$  are caused by small changes in  $x, y$ . The rate at which these changes occur is irrelevant.

### Change of variable.

$x, y$  can be expressed in terms of polar coordinates,  $r, \theta$ . We have



$$df = \frac{\partial f}{\partial x} dx + \frac{\partial f}{\partial y} dy$$

$$dx = \frac{\partial x}{\partial r} dr + \frac{\partial x}{\partial \theta} d\theta$$

$$dy = \frac{\partial y}{\partial r} dr + \frac{\partial y}{\partial \theta} d\theta$$

$$\text{So } df = \frac{\partial f}{\partial x} \left( \frac{\partial x}{\partial r} dr + \frac{\partial x}{\partial \theta} d\theta \right) + \frac{\partial f}{\partial y} \left( \frac{\partial y}{\partial r} dr + \frac{\partial y}{\partial \theta} d\theta \right)$$

$$= dr \left( \frac{\partial f}{\partial x} \frac{\partial x}{\partial r} + \frac{\partial f}{\partial y} \frac{\partial y}{\partial r} \right) + d\theta \left( \frac{\partial f}{\partial x} \frac{\partial x}{\partial \theta} + \frac{\partial f}{\partial y} \frac{\partial y}{\partial \theta} \right)$$

$$\frac{\partial f}{\partial r} = \frac{\partial f}{\partial x} \frac{\partial x}{\partial r} + \frac{\partial f}{\partial y} \frac{\partial y}{\partial r}$$

$$\frac{\partial f}{\partial \theta} = \frac{\partial f}{\partial x} \frac{\partial x}{\partial \theta} + \frac{\partial f}{\partial y} \frac{\partial y}{\partial \theta}$$

Corresponds to chain rule. We have  $\frac{\partial f}{\partial r} = \frac{df}{dr}$  and in spaces, variables corresponding to the different routes by which  $r$  can influence  $f$ .

Note: we cannot cancel  $\frac{\partial x}{\partial r}$  and  $\frac{\partial y}{\partial r}$  in this world since  $\frac{\partial f}{\partial r} = 2 \frac{\partial f}{\partial r}$ .

PD 3  
P16

$$x = r \cos \theta \quad y = r \sin \theta$$

$$\frac{\partial f}{\partial r} = \frac{\partial f}{\partial x} \cos \theta + \frac{\partial f}{\partial y} \sin \theta$$

$$\frac{\partial f}{\partial \theta} = \frac{\partial f}{\partial x} (-r \sin \theta) + \frac{\partial f}{\partial y} (r \cos \theta)$$

[Set] Example. Consider  $f = x^2 + y^2$   $\frac{\partial f}{\partial x} = 2x$   $\frac{\partial f}{\partial y} = 2y$ .

$$\frac{\partial f}{\partial r} = 2x \cos \theta + 2y \sin \theta = 2r \cos^2 \theta + 2r \sin^2 \theta = 2r.$$

$$\frac{\partial f}{\partial \theta} = 2x(-r \sin \theta) + 2y(r \cos \theta)$$

$$= 2r \cos \theta (-r \sin \theta) + \cancel{2r \sin \theta} 2r \sin \theta (r \cos \theta) = 0$$

as it should.

Partial Differentiation.

$f(x, y)$ .  $\frac{\partial f}{\partial x}$  is rate of increase when  $x$  grows at unit rate,  $y$  held constant.  $\frac{\partial f}{\partial y}$  is rate of increase when  $y$  grows at unit rate,  $x$  held constant.

These are sometimes denoted by  $\frac{\partial f}{\partial x}|_y$  and  $\frac{\partial f}{\partial y}|_x$ , the  $|_x$  and  $|_y$  showing what is held constant.

In (1) the following situation  $x$  is growing, but in (2)  $y$  is held constant, & (2)  $y-x$  is held constant.



(1) would arise naturally if we have  $z = f(x, y)$

(2) if  $z = \cancel{f(x, y)}$   $\bar{z} = f(\gamma, u)$  with  $u = y - x$ .

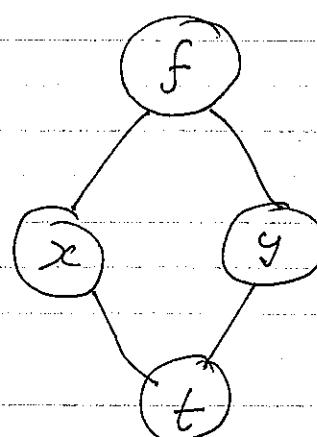
In physics this arises for a gas, temperature rising with constant pressure has different effect from temperature rising at constant volume (gas held in solid container).

In the first case, heat supplied has two parts - that used to raise the temperature, and that doing work to cause expansion.

In the second case, all the heat is used to raise temperature.

If  $f = f(x, y)$  and  $x$  and  $y$  are increasing at rate,  $\frac{dx}{dt}, \frac{dy}{dt}$

we may picture  $f$  as given by a meter ready, the value of which depends on the settings of 2 dials. If a clock is geared to these so that  $x$  and  $y$  increase in a specified way,  $f$  will increase (or decrease). The behaviour of  $f$  is determined.



If  $x$  increases at rate  $\frac{dx}{dt}$ ,  $f$  P changes at rate  $\frac{\partial f}{\partial x} \frac{dx}{dt}$

$$y = - - - \frac{\frac{\partial f}{\partial x} dx}{\frac{\partial f}{\partial y} dy}$$

In many situations (not all), if  $x$  and  $y$  vary simultaneously

$$\frac{df}{dt} = \frac{\partial f}{\partial x} \frac{dx}{dt} + \frac{\partial f}{\partial y} \frac{dy}{dt}. \quad (1)$$

[This result is equivalent to  $z = f(x, y)$  having a tangent plane at the point  $(x_1, y_1, z_1)$ .]

It is often convenient to write eqn (1) as

$$df = \frac{\partial f}{\partial x} dx + \frac{\partial f}{\partial y} dy. \quad (2)$$

The chain rule  $\frac{dy}{dx} = \frac{dy}{dz} \frac{dz}{dx}$  looks as if it is a result in algebra. Note that (1) does not. We cannot cancel  $dx$  and  $dy$ , etc.

$\frac{\partial f}{\partial x} \frac{dx}{dt}$  is that part of  $\frac{df}{dt}$  due to the change in  $x$ ;  $\frac{\partial f}{\partial y} \frac{dy}{dt}$  that part due to  $y$  varying.

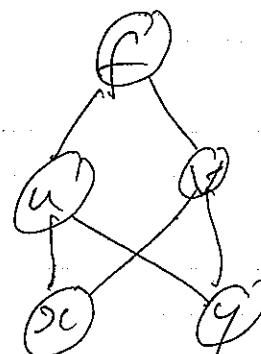
### Change of variable

Let  $f = f(u, v)$  where  $u$  and  $v$  are functions of  $x$  and  $y$ .

$$df = \frac{\partial f}{\partial u} du + \frac{\partial f}{\partial v} dv$$

$$du = \frac{\partial u}{\partial x} dx + \frac{\partial u}{\partial y} dy$$

$$dv = \frac{\partial v}{\partial x} dx + \frac{\partial v}{\partial y} dy$$



Substituting gives

$$\begin{aligned} df &= \frac{\partial f}{\partial u} \left( \frac{\partial u}{\partial x} dx + \frac{\partial u}{\partial y} dy \right) + \frac{\partial f}{\partial v} \left( \frac{\partial v}{\partial x} dx + \frac{\partial v}{\partial y} dy \right) \\ &= \left( \frac{\partial f}{\partial u} \frac{\partial u}{\partial x} + \frac{\partial f}{\partial v} \frac{\partial v}{\partial x} \right) dx + \left( \frac{\partial f}{\partial u} \frac{\partial u}{\partial y} + \frac{\partial f}{\partial v} \frac{\partial v}{\partial y} \right) dy \end{aligned}$$

$$\text{So } \frac{\partial f}{\partial x} = \frac{\partial f}{\partial u} \frac{\partial u}{\partial x} + \frac{\partial f}{\partial v} \frac{\partial v}{\partial x}; \frac{\partial f}{\partial y} = \frac{\partial f}{\partial u} \frac{\partial u}{\partial y} + \frac{\partial f}{\partial v} \frac{\partial v}{\partial y}$$

When  $x$  changes, part of the effect is via  $u$ , part via  $v$ .

Edwards. p 125 No 4.

If  $x = r \cos \theta$  and  $y = r \sin \theta$  prove  
 $dx = \cos \theta dr - r \sin \theta d\theta$   
 $dy = \sin \theta dr + r \cos \theta d\theta$

Deduce  $dx^2 + dy^2 = dr^2 + r^2 d\theta^2$

$x dy - y dx = r^2 d\theta$ .

But why?  $ds^2 = \frac{1}{r^2} r^2 d\theta$  is area swept out.

C, A points on curve.

$OC = r \angle AOC = d\theta$

$MN = x \quad AB = dy$

$x dy = \square PBAM$

$= 2 \Delta OAB$

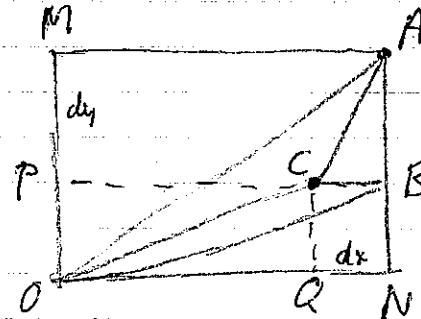
$y dx = \square CBNC$

$= 2 \Delta OBC$

$x dy - y dx = 2 (\Delta OAB - \Delta OBC) = 2 (\Delta OAC + \Delta ACB)$

$2 \Delta ACB = dx dy$ . 2nd order.

Note we have taken MA as  $x$ . Perhaps it should be  $x dy$ .  
 This would account for an extra  $dx dy$ .



5) If  $u = \ln(x^2 + y^2 + z^2)$  prove

$$\frac{\partial u}{\partial y \partial z} = 4 \frac{\partial u}{\partial z \partial x} = 3 \frac{\partial^2 u}{\partial x \partial y}$$

(5)  $u = \ln(x^2 + y^2 + z^2)$

$$du = \frac{2x dx + 2y dy + 2z dz}{x^2 + y^2 + z^2}$$

$$\frac{\partial u}{\partial x} = \frac{2x}{x^2 + y^2 + z^2}$$

$$\frac{\partial^2 u}{\partial x \partial y} = \frac{2(x^2 + y^2 + z^2) - 2x^2 - 2y^2}{(x^2 + y^2 + z^2)^2}$$

$$= \frac{-2x(2y)}{(x^2 + y^2 + z^2)^2} = \frac{-4xy}{(x^2 + y^2 + z^2)^2}$$

$$\therefore 3 \frac{\partial^2 u}{\partial x \partial y} = -\frac{4xy^3}{(x^2 + y^2 + z^2)^2} \text{ sign Q.E.D}$$

(6) If  $\frac{x^2}{a^2} + \frac{y^2}{b^2} = 1$  prove  $\frac{dy}{dx} = -\frac{b^2 x}{a^2 y}$   $\frac{d^2 y}{dx^2} = -\frac{b^4}{a^2 y^3}$

If  $f(x, y) = \cosh \frac{df}{dx} + \frac{\partial f}{\partial y} = 0 \therefore \frac{dy}{dx} = -\frac{\partial f / \partial x}{\partial f / \partial y}$

For  $f(x, y) = \frac{x^2}{a^2} + \frac{y^2}{b^2}$   $\frac{\partial f}{\partial x} = \frac{2x}{a^2}$   $\frac{\partial f}{\partial y} = \frac{2y}{b^2}$  Hence (i)

$$b^2 x + a^2 y y' = 0$$

$$b^2 + a^2(y'' + y'^2) = 0$$

$$\therefore a^2 y'' = -b^2 - a^2 y'^2$$

$$\therefore y'' = -\frac{b^2}{a^2 y} - \frac{y'^2}{y}$$

$$= -\frac{b^2}{a^2 y} - \frac{b^4 x^2}{a^4 y^3} = \frac{a^2 b^2 y^2 + b^4 x^2}{a^4 y^3}$$

$$= -\frac{a^2 b^2}{a^2 y^4} \left( \frac{y^2}{a^2} + \frac{x^2}{b^2} \right)$$

$$= -\frac{b^4}{a^2 y^3}$$

or  $y' = -\frac{b^2 x}{a^2 y}$

$$y'' = -\frac{b^2 x y - a^2 y^2 b^2 x}{a^2 y^3} \quad y' = -\frac{b^2 x}{a^2 y}$$

Approximations to  $\frac{dy}{dx}$  and  $\frac{d^2y}{dx^2}$ .

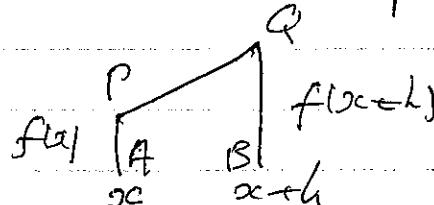
P21

A computer may give us a table for  $y = f(x)$  but not the analytic formula. If we wish to do some work involving  $f'(x)$  and  $f''(x)$  we have to use approximations and hope these will work well.

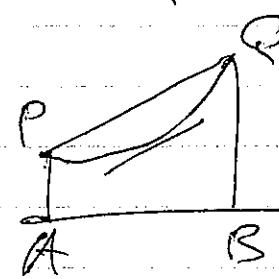
$$f'(x) = \lim_{h \rightarrow 0} \frac{f(x+h) - f(x)}{h}.$$

If we have a table of  $f(x)$  at intervals  $h$ , we naturally consider  $\frac{f(x+h) - f(x)}{h}$  as a suitable approximation.

This is the gradient of PQ. It may very well give the gradient at some points between A and B.

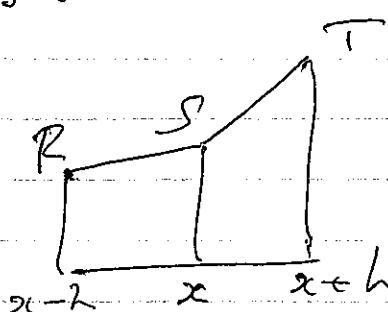


If  $h$  is extremely small, and we have reason to believe that the gradient varies gradually we might even take it as  $\text{avg } f'(x)$  at A.



$f''(x)$

The approximation here is slightly less arbitrary.



$f''(x)$  is the rate of change of  $f'(x)$ .

$\frac{f(x) - f(x-h)}{h}$  is an estimate for  $\frac{dy}{dx}$  at CD,

$\frac{f(x+h) - f(x)}{h}$  is an estimate for  $\frac{dy}{dx}$  at ST.

This leads to the estimate

$$f''(x) = \frac{f(x+h) - 2f(x) + f(x-h)}{h^2}.$$

Note. This is  $\frac{\Delta^2 f}{(2\Delta x)^2}$ .

We can use this approximation to make plausible  
- not to prove - various results in physics.

Vibrating wire, loaded with masses.

Tension  $T$  unaltered.

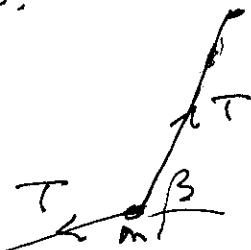
Force on mass  $m$  is

$$T \sin \beta - T \sin \alpha$$

$$\Rightarrow T \tan \beta - T \tan \alpha$$

$$= T \frac{f(x+h) - f(x)}{h} - T \frac{f(x) - f(x-h)}{h}$$

$$= T \frac{f(x+h) - 2f(x) + f(x-h)}{h}$$



If masses are at intervals  $h$  the mass per unit length  $\rho = m \cdot \frac{1}{h} =$

Acceleration per  $h$

$$m \frac{\partial^2 y}{\partial t^2} = T \frac{f(x+h) - 2f(x) + f(x-h)}{h}$$

$$\therefore \rho \frac{\partial^2 y}{\partial t^2} = \frac{m}{h} \frac{\partial^2 y}{\partial t^2} = T \frac{f(x+h) - 2f(x) + f(x-h)}{h^2}$$

$$\therefore T \frac{\partial^2 y}{\partial x^2}$$

~~If  $c = \sqrt{\frac{T}{\rho}}$ ,  $\frac{\partial^2 y}{\partial t^2} = c^2 \frac{\partial^2 y}{\partial x^2}$~~  If  $c^2 = \frac{T}{\rho}$ ,  $\frac{\partial^2 y}{\partial x^2}$

$$\frac{\partial^2 y}{\partial x^2} = \frac{1}{c^2} \frac{\partial^2 y}{\partial t^2}$$

Dimensions:  $\rho = M/L$ .  $T = \text{force} = \text{mass} \times \text{accel}'$   
 $= M L T^{-2}$

$$\therefore c^2 = \frac{T}{\rho} = \frac{M L T^{-2}}{M/L} = L^2 T^{-2}$$

$L T^{-1}$  is velocity.  $c$  has the dimensions of a velocity.

Other applications left for the moment.

4

P23

Change of variable in  $\frac{\partial^2 y}{\partial x^2} = \frac{1}{c^2} \frac{\partial^2 y}{\partial t^2}$ .

Let  $u = x + ct$ .

$$v = x - ct.$$

$$\frac{\partial}{\partial x} = \frac{\partial u}{\partial x} \frac{\partial}{\partial u} + \frac{\partial v}{\partial x} \frac{\partial}{\partial v} = \frac{\partial}{\partial u} + \frac{\partial}{\partial v}.$$

$$\frac{\partial}{\partial t} = \frac{\partial u}{\partial t} \frac{\partial}{\partial u} + \frac{\partial v}{\partial t} \frac{\partial}{\partial v} = c \frac{\partial}{\partial u} - c \frac{\partial}{\partial v}$$

$$\therefore \frac{\partial^2}{\partial x^2} - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} = \left( \frac{\partial}{\partial u} + \frac{\partial}{\partial v} \right)^2 - \left( c \frac{\partial}{\partial u} - c \frac{\partial}{\partial v} \right)^2 \\ = 4 \frac{\partial^2 u}{\partial u \partial v}$$

$$\therefore \frac{\partial^2 y}{\partial u \partial v} = 0$$

What is meaning of such an equation?

Consider 1)  $\frac{\partial f}{\partial x} = 0$

2)  $\frac{\partial f}{\partial y} = 0$

3)  $\frac{\partial^2 f}{\partial x \partial y} = 0$ .

$$(2x-5)(3x+4) = 6x^2 - 7x - 20$$

$$6x^2 - 7x - 20 = 0$$

$$6x^2 - 7x = 20$$

$$x^2 - \frac{7}{6}x = \frac{20}{6} = \frac{10}{3}$$

$$\left(x - \frac{7}{12}\right)^2 = \frac{10}{3} + \frac{49}{144} = \frac{480 + 49}{144} = \frac{9}{144}$$

Very thought Factors are seen after. Answer the  
 Period is seen. Period is  $\frac{\pi}{2}$

$$u = x + ct$$

$$v = x - ct$$

$$\frac{\partial}{\partial x} = c \frac{\partial}{\partial u} + \frac{\partial}{\partial v}$$

$$\frac{\partial}{\partial t} = c \frac{\partial}{\partial u} - c \frac{\partial}{\partial v}$$

$$\left(\frac{\partial}{\partial x}\right)^2 - c^2 \left(\frac{\partial}{\partial u}\right)^2$$

## Paradoxes of Classical Physics.

### 1. The existence of atoms.

The stability of chemical compounds led chemists to believe in a static model of the atom. When it became accepted that electrons moved in orbits, a difficulty arose. An ~~moving charge emits~~ accelerating charge ~~radiates~~ causes radiation and thus loses energy. An electron in orbit around a nucleus should lose energy and spiral inward, until it collided with the nucleus.

### 2. Line spectra

Very often the spectrum of an atom contains lines. Each line corresponds to a particular frequency. Classical theory had no way of explaining why certain frequencies should be picked out as special.

### 3. The photoelectric effect.

When light (or other radiation) falls on a solid it may cause electrons to be emitted. The way in which this happened was puzzling. If the frequency of the light was below a certain value, no electrons came however intense the illumination. When the frequency is sufficient to cause the emission of electrons, the maximum kinetic energy of the emerging electrons cannot be increased by more intense illumination. The effect is that more electrons emerge per second. The kinetic energy does increase if the ~~higher~~ frequency of the light increases.

### 4. Black body radiation

A body is "black" when it absorbs all radiation falling on it. A heated body with a cavity is used. Radiation enters through a tiny hole. It is partly absorbed, partly reflected many times. The chance of its emerging is very small.



If the cavity is heated to, say, red heat, a small amount of radiation will emerge from the hole. This is studied as "black body radiation".

Q 2

Radiation in a heated cavity can be studied by the methods of statistical mechanics. Rather as for a vibrating string, various simple modes are possible.



We can have  $n$  parts such as  $\nearrow$  or  $\searrow$ . On classical theory, each such vibration has the same energy  $\epsilon$ .

How many oscillations have wavelength in  $\lambda - \epsilon$  to  $\lambda$ ?

$$\text{If } \lambda = \frac{t}{n} \text{ and } \lambda - \epsilon = \frac{t}{m}, m = \frac{1}{\lambda - \epsilon}, n = \frac{1}{\lambda}$$

$m - n = \frac{\epsilon}{\lambda(\lambda - \epsilon)}$ . If  $\epsilon$  is small, this is approximately  $\epsilon/\lambda^2$ . Thus the number of modes lying between  $n$  and  $m$  is much larger for small  $\lambda$ .

In fact, there are an infinity of modes, and only a finite number of these have  $\lambda \geq a$ , for any  $a$ .

Thus energy is concentrated in the very short waves.

The Rayleigh-Tamm calculation showed that in fact the energy  $\epsilon_\lambda d\lambda = C T \lambda^{-4} d\lambda$ . This fits the experimental data only for large wavelengths.

Correspondence principle — classical theory works all right for large or slow phenomena. They new theory should agree with old in such situations.

Planck seems to have found it mathematically convenient to use an argument in which the energy of any vibrator had to be  $0, \epsilon, 2\epsilon, 3\epsilon, \dots$  with the invention of letting  $\epsilon \rightarrow 0$  at the end of the calculation. However, he found he could get a better result by not taking this limit.

$$\text{He found } \epsilon_\lambda d\lambda = 8\pi t^{-4} \frac{\epsilon}{e^{\epsilon/kT} - 1} d\lambda \quad (1)$$

If  $\epsilon$  is small,  $e^{\epsilon/kT} \approx 1 + \epsilon/kT$  and the result is  $8\pi kT \lambda^{-4}$ , the Rayleigh-Tamm calculation.

Thermodynamic reasoning had shown that the formula ought to have the form  $C \lambda^{-5} f(\lambda T) d\lambda \quad (2)$  for some function  $f$ .

Two differences: (1) has  $\lambda^{-4}$ , (2) has  $\lambda^{-5}$ . Both differences disappear if we take  $\epsilon = \lambda/kT$ . Then we have

$$8\pi \lambda^{-5} \frac{\epsilon}{e^{\epsilon/kT} - 1} d\lambda. \quad (3)$$

If we have a long wavelength,  $\lambda$  is large,  $\alpha/k\lambda T$  is small and  $e^{\alpha/k\lambda T} \approx 1 + \frac{\alpha}{k\lambda T}$

$$\text{Thus } (3) \rightarrow 8\pi\lambda^{-5} \cdot \frac{\alpha d\lambda}{\left(\frac{\alpha}{k\lambda T}\right)} = 8\pi k \lambda^{-4} d\lambda,$$

The Rayleigh Jeans result. So the Correspondence Principle is satisfied: the classical result checks for long wavelengths.

Wave length  $\lambda$  now occurs with packets of energy  $\Sigma = \alpha/\lambda$  at  $\lambda = c/\nu$ , where  $\nu$  is the frequency,  $\Sigma = \alpha\nu$ . Putting  $\hbar = c/e$ , the packet is  $\hbar\nu$ , where  $\hbar$  is Planck's constant.

We have a paradox: light behaves like waves: it also behaves like a hail of bullets.

This explains the photoelectric effect. light of frequency  $\nu$  corresponds to bullets of energy  $\hbar\nu$ . If this energy is not enough to knock an electron out of a metal, no photo-electrons will appear however intense the light. Greater intensity means more bullets but as each bullet is ineffective, this makes no difference.

If the energy is enough to knock the electron out, the maximum velocity of electrons emerging is not increased by increasing the light intensity, - only the frequency with which electrons emerge.

This explanation was given by Einstein in 1905.

The Bohr model of the atom.

The next step forward after Planck was a very remarkable piece of thinking and quite as revolutionary.

The following considerations may prepare you for it.

Planck's basic assumption was that a simple oscillator with frequency  $\nu$  could have energy  $0, h\nu, 2h\nu, \dots$ . If  $x = a \cos(\omega t / 2\pi)$  describes its motion the energy is  $\frac{1}{2}m\left(\frac{\omega a}{2\pi}\right)^2$ , thus  $a^2$  can have the values

$$\frac{8\pi^2}{m\nu^2} \cdot n h\nu = n \frac{8\pi^2 h}{m\nu^2}$$

Thus the possible vibrations can have only certain amplitudes

$$\begin{array}{c} \leftrightarrow \\ \leftrightarrow \\ \leftrightarrow \end{array} \begin{array}{l} n=1 \\ n=2 \\ n=3 \end{array}$$

Suppose we have a particle that can oscillate in the  $x$ -direction and in the  $y$ -direction. If  $n=3$  for the  $x$  oscillation and  $n=2$  for the  $y$  oscillation it will describe a path



There will be other possible paths singled out by the conditions.

Bohr postulated that, for the motion of an electron about a proton, certain orbits were singled out. On classical theory, an electron moving in an orbit would radiate energy and move in towards the proton. Bohr maintained that this was not so.

The orbits were stable. An electron could remain in an orbit for a considerable time.

However it was possible for an electron to cease to be in an orbit, and appear instead in a lower orbit with less energy. Radiation would be emitted. The frequency of the radiation would not bear any relationship to the velocity or acceleration of the electron in either orbit. It would be determined by the conservation of energy. A photon (pulse of light) with frequency  $\nu$  has energy  $h\nu$ . ~~The~~

If the electron falls from an orbit of energy  $E_1$  to an orbit of energy  $E_2$ , then  $E_1 - E_2 = h\nu$ .

If the electron is in the orbit with least energy it cannot fall further. Thus atoms can survive.

The theory explains why the spectrum contains separate lines. On classical theory it would be continuous.

When radiation is absorbed, it can kick an electron to a higher level

The quantum conditions

A very simple case is that of a mass  $m$  describing a circle of radius  $r$  with constant velocity,  $v = r\omega$

The angular momentum  $rv = r^2\omega$ . The mass returns to the same position when  $\omega$  changes by  $2\pi$ .

The quantum condition is  $2\pi r^2 \omega m = nh$ . (1)

From dynamics  $mr\omega^2 = e^2/r^2$  (2)

$$\text{From (1), } \omega^2 = \frac{n^2 h^2}{4\pi^2 m^2 r^4}$$

Substitute in (2)

$$\frac{mr^2 \cdot h^2}{4\pi^2 m^2 r^4} = \frac{e^2}{r^2}$$

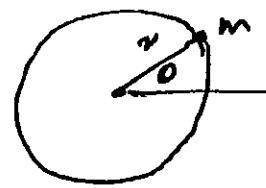
$$\therefore r = \frac{n^2 h^2}{4\pi^2 m e^2}$$
(3)

$$\begin{aligned} E &= \frac{1}{2} mr^2 \omega^2 - \frac{e^2}{r} \\ &= \frac{1}{2} mr^2 - \frac{e^2}{mr^3} - \frac{e^2}{r} \quad \text{from (2)} \\ &= \frac{e^2}{2r} - \frac{e^2}{r} = -\frac{e^2}{2r} \\ \text{So } E &= -\frac{4\pi^2 m e^4}{2n^2 h^2} = -\frac{2\pi^2 m e^4}{n^2 h^2}. \end{aligned}$$

The lines in the spectrum fit

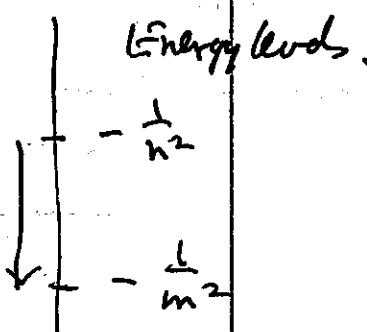
$$\text{frequency} = c \left( \frac{1}{m^2} - \frac{1}{n^2} \right) \text{ where } n < m.$$

This is a fall in energy when radiation is emitted, a rise when radiation is absorbed.



Q8.

P29



In a hydrogen atom, the position of an electron requires 3 numbers to specify it.

- 1 the distance from the origin.
- 2 the co-latitude
- 3 the longitude.

If the electron describes an orbit all in a plane not perpendicular to  $\vec{O}\vec{r}$ , all three variables are periodic; they return to their initial values when the electron has returned to its initial position.

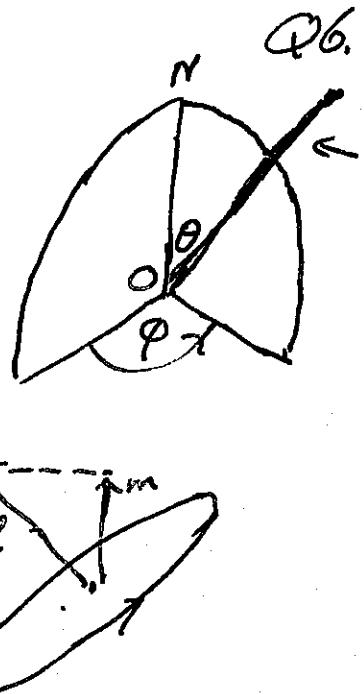
Bohr found conditions for the orbits to be permissible, which gave 3 quantum numbers,  $n$  associated with  $r$ ,  $l$  associated with  $\theta$ ,  $m$  associated with  $\phi$ .

The total quantum number,  $n = n' + l + 1$  is important. The energy is proportional to  $-1/r^2$ .

$$\begin{aligned} n &\text{ can be } 1, 2, 3, \dots \\ l & \quad \quad \quad 0, 1, \dots, n-1. \\ m & \quad \quad \quad -l, -l+1, \dots, 0, \dots, l-1, l. \end{aligned}$$

In an atom with several electrons, it is no longer possible to find exact expressions for the orbits or for the energy, but it is assumed that each electron has numbers  $n, l, m$  and also a spin number  $\pm \frac{1}{2}$ .

Pauli exclusion principle: two electrons cannot have all their numbers identical.



Q6.

The fact that  $s$  can be  $+\frac{1}{2}$  or  $-\frac{1}{2}$  means that if  $n, l, m$  have been fixed, there are just 2 possibilities.

Thus, we can forget about  $s$  if we allow every number system  $n, l, m$  to be taken twice.

Lowest order If  $n=1, l=0, m=0$ . Two atoms can be accommodated at this level.

	$n = 1$
	$l = 0$
H	1
He	2

Choices for  $m$ :  $-l \leq m \leq l$ . For given  $l$ , there are  $2l+1$  choices for  $m$ .

Double this, to allow for  $s = \pm\frac{1}{2}$ , we have  $2(2l+1)$ .

Thus, with  $l=0$  we have niches for 2 atoms.

$l=1$	6
$l=2$	10

To begin with, these niches are filled in a quite systematic way.

	1	2	1	3	4	
$l$	0	0	1	0	1	2
H	1					
He	2					
Li	2	1				
Be	2	2				
B	2	2	1			
C	2	2	2			
N	2	2	3			
O	2	2	4			
F	2	2	5			
Ne	2	2	6			
Na				1		
Mg				2		
Al				2	1	
Si				2	2	
P				2	3	
S				2	4	
Cl				2	5	
Ar				2	6	

Notice the similarity  
in the outside shells.

This part  
says the same

At the next stage we would expect to find  $n=3$ ,  $l=2$   
filling up. But it does not happen like that.

Q8

P  
32

	1	2	3	4				
$l$	0	0	1	0	1	2	0	1
K	2	2	6	2	6		1	
Ca							2	
Sc					1		2	
Ti					2		2	
V					3		2	
Cr					5	1		
Mn					5	2		
Fe					6	2		
Co					7	2		
Ni					8	2		
Ca					10	1		
Zn					10	2		
Ga					10	2	1	
Ge					10	2	2	
As					10	2	3	
Se					10	2	4	
Br					10	2	5	
Kr					10	2	6	

The transition elements are the most industrially important metals and this is mainly due to the presence of strong interatomic bonding forces which results in them having high melting points and good mechanical properties.

Lipkin. P 350  
Modern Inorganic Chemistry.

See also Durrant General and Inorganic Chemistry p 157

B P<sub>33</sub>

If sequence  $a_0, a_1, \dots, a_n$  is to have the property that 0 occurs in it  $a_0$  times, 1 occurs  $a_1$  times and so,  $n$  occurring  $a_n$  times. An example is

$a_0$	0	1	2	3	4	5	6	7	8
$a_{n+1}$	5	2	1	0	0	1	0	0	0

The sum of the numbers in the sequence, found by considering how many times each of 0, 1, ...,  $n$  occurs, is  $a_0(0) + a_1(1) + a_2(2) + \dots + a_n(n)$ . But the sum is  $a_0 + a_1 + a_2 + \dots + a_n$ .

Equating these we have  $a_0 = a_2 + 2a_3 + 3a_4 + \dots + (n-1)a_n$ . (1)

It follows that  $a_3, a_4, \dots, a_n$  are all less than  $a_0$ . Also  $a_2 < a_0$  unless  $a_3, \dots, a_n$  are all 0, and then  $a_2 = a_0$ . We first consider this exceptional case.

The sequence  $a_0, a_1, a_2, 0, \dots, 0$ .

Let  $a_2 = a_0 = k$ ,  $a_1 = m$ . The numbers in the sequence are selected from 0, 1, 2. The number of non-zero numbers in the sequence is  $k+m$ . This cannot be 3, for then this cannot exceed 3, since only  $a_0, a_1, a_2$  can be other than 0.

As  $a_3=0, a_4=0, \dots$  no number larger than 2 can occur in the sequence.  $k=0$  is ruled out, since this would say no 0 occurs, and at the same time say  $a_0=0$ . These conditions allow 5 possible

sequences. (a) 101... (b) 111... (c) 121 (d) 202.  
(e) 201 212

(a) and (e) must be ruled out: they say no 1 occurs, but it does. (b) falsely claims the presence of 2.

(c) gives 1210 and (d) gives 2020  
both of which are solutions

## The General Case.

The general case occurs is that when  $a_3 \dots a_n$  are not all zero. Equation (5) shows that  $a_0$  is at least 2, so  $a_0 \neq 1$ . We have shown that  $a_0$  is larger than any number in the sequence except possibly  $a_1$ .

P.34

We proceed to eliminate certain possibilities. As before, let  $a_0 = k$ ,  $a_1 = m$ .

We show  $a_0 \neq a_1$ . If  $m = k$ , all the other numbers in the sequence being less than  $k$  we have  $a_{k+1} \geq 2$ . Thus neither  $a_0$  nor  $a_k$  can be 1. The sites where 1 can occur

~~are~~ we know  $a_0 \neq 1$ , ~~a~~. Also  $a_1 = m$ ,

and  $m = k > 1$ . So  $a_0$ ,  $a_1$  and  $a_k$  are not places available for 1. This leaves

$a_2 \dots a_{k-1}$ , only  $k-2$  possible sites, so  $a_1$  cannot exceed  $k-2$ . There is a contradiction in supposing  $a_1 = k$ .

We also show  $a_1$  is not greater than  $k$ . If it were we would have  $a_k = 1$ ,  $a_m = 1$ .

We try to fit  $m-2$  "1's" ~~thus  $m-2$~~  endings of 1 must occur for  $a_r$  with  $r < k$ . If all the other numbers are less than  $k$ , we cannot find  $a_r = 1$  with  $r > k$  except for  $r = m$ . The only places where 1 can occur are  $a$ .  $a_1 > k > 1$  excludes the possibility that  $a_1 = 1$ . Thus the possible sites possible for  $a_r = 1$  are  $a_2 \dots a_{k-1}$ . There are  $k-2$  in number. 1 must occur in times in all, so it must occur  $m-2$  times apart from  $a_{k+1}$  and  $a_m$ . So  $m-2$  cannot exceed  $k-2$ , which means  $m$  cannot exceed  $k$ . This contradicts the initial hypothesis  $m > k$ .

Accordingly  $a_1 \leq a_0$ .

1  
R1

Object in circle

radius  $R$

$\varphi$  angle between target  
and fixed direction

Angle at center is  $\varphi_2 - \varphi_1$

$$\text{arc} = R(\varphi_2 - \varphi_1)$$

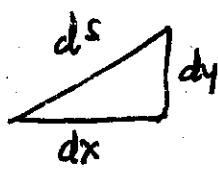
$$ds = R d\varphi \quad R = \frac{ds}{d\varphi}$$

For a circle  $\frac{ds}{d\varphi}$  is constant.

For any curve  $\frac{ds}{d\varphi}$  gives a measure of  
the curvature at that point, the radius of  
the circle that this part of the curve resembles.

We define  $\rho = \frac{ds}{d\varphi}$ , the "radius of curvature."

Formula for  $\rho$  in Cartesian co-ordinates.



$$ds^2 = dx^2 + dy^2$$

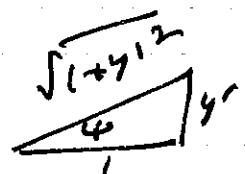
$$\left(\frac{ds}{dx}\right)^2 = 1 + \left(\frac{dy}{dx}\right)^2$$

$$\frac{ds}{dx} = \sqrt{1 + y'^2}$$

$$y' = \tan \varphi$$

$$\varphi = \tan^{-1} y'$$

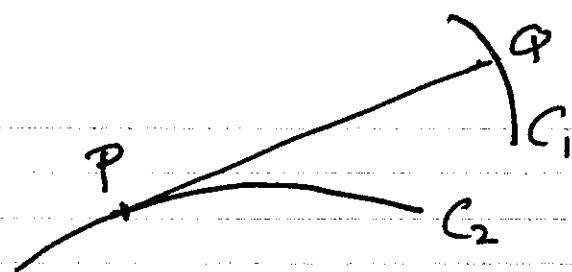
$$\frac{dy}{dx} = \sec^2 \varphi \cdot \frac{d\varphi}{dx}$$



$$\frac{d\varphi}{dx} = \frac{y''}{\sec^2 \varphi} = \cos^2 \varphi \cdot y'' = \frac{y''}{1 + y'^2}$$

$$\rho = \frac{ds}{d\varphi} = \frac{ds/dx}{d\varphi/dx} = \frac{\sqrt{1+y'^2}}{\left(\frac{y''}{1+y'^2}\right)} = \frac{(1+y'^2)^{3/2}}{y''}$$

$\frac{2}{R_2}$



If we pull curve  $C_1$  by unthreading a thread from curve  $C_2$  it looks as if  $PQ$  is normal to curve  $C_1$  at  $Q$ ,  $PQ$  is tangent to curve  $C_2$  at  $P$  and  $P$  is the centre of circle resembling the curve  $C_1$  at  $Q$ .

It is good to verify intuitive ideas analytically.

We need to show that, if a little later we have  $P'$  and  $Q'$ , then in the limit

$P'P =$  the increase in  $P$

$P'P$  should be in line with  $PQ$ .

$P(X, Y)$

Centre of curvature is distance  $p$  along the normal from  $Q$ .

Curve  $C_2$  is to be the locus of centre of curvature.

Let  $P$  be  $(X, Y)$

$$X = x - p \sin \varphi$$

$$Y = y + p \cos \varphi$$

We want to show that in an infinitesimal change, centre of curvature moves in direction  $QP$ , and a distance  $dp$ .

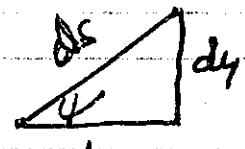
$$dX = dx - dp \sin \varphi - p \cos \varphi dy$$

$$dY = dy + dp \cos \varphi - p \sin \varphi dx$$

$$P = \frac{dx}{dy} \quad pdy = ds$$

$$-p \cos \varphi dy = -ds \cos \varphi$$

$$= -dx$$



R 3

$$\therefore \underline{dx = -dp \sin \psi}$$

$$-p \sin \psi dy = -\frac{ds}{d\psi} \sin \psi dy$$

$$= -ds \sin \psi = -dy$$

$$\therefore \underline{dy = dp \cos \psi}$$

So  $(dx, dy)$  represents a distance  $dp$   
along normal. Q. E. D.

A possible construction for the evolute  
(locus of centres of curvature)

R4

Radius of curvature.

If a particle is moving in a circle of radius  $R$ ,



and  $\varphi$  is angle between tangent and a fixed director,  $R d\varphi = ds$

$$\text{so } R = \frac{ds}{d\varphi}.$$

For a curve that is not a circle we take  $\rho = \frac{ds}{d\varphi}$  as the instantaneous radius of curvature. This would, for example, allow us to estimate the speed at which a car could be driven at that point, by comparing it to driving round a circle with that radius.  $\rho$  is called "radius of curvature".

$\rho$  in terms of  $x, y$ .

$$\tan \varphi = \frac{dy}{dx} \quad \varphi = \tan^{-1} y'$$

$$\therefore \frac{ds}{dx} = \frac{1}{(1+y'^2)} \cdot y''$$

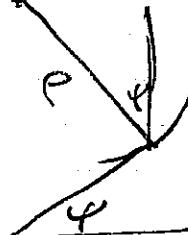
$$\frac{ds}{dx} = \sqrt{1+y'^2}$$

$$\therefore \frac{ds}{dt} = \frac{(1+y'^2)^{3/2}}{y''} = \rho.$$

Centre of curvature is reached by going a distance  $\rho$  along the normal.

$$x = x - \rho \sin \varphi$$

$$y = y + \rho \cos \varphi.$$



## Set. Sets, Open & Closed

~~RS~~ S 1

Neighbourhood supposed defined.

Neighbourhood of a point  $P = \{Q : \|PQ\| < k\}$  for some  $k > 0$ .

limit point of set  $S$ .  $P$ , such that any neighbourhood of  $P$  contains points of  $S$  other than  $P$ . It does not matter whether  $P \in S$  or not.

Example  $S_1 = \{x : |x| < 1\}$   $x=1$  is a limit point.

$1$  is still a limit point

if  $S_2 = \{x : |x| \leq 1\}$

In fact every point of  $S_1$  is a limit point of  $S_2$ .

Same for  $S_2$ .

There must be  $\infty$  points in a neighbourhood of a limit point.

Proof Suppose that a neighbourhood contains only

$Q_1, Q_2, \dots, Q_n$ .

Then  $P$  cannot be a

limit point.

$k < \min\{|PQ_1|, |PQ_2|, \dots, |PQ_n|\} \{ |PQ_1|, |PQ_2|, \dots, |PQ_n|\}$

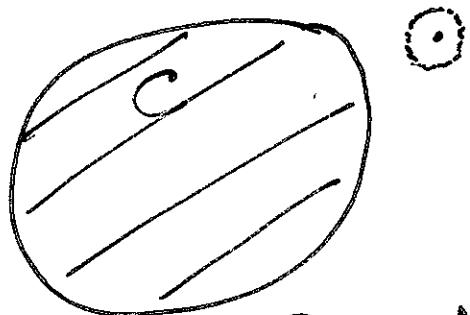
Closed set.  $S$  is closed if it contains all its limit points.

Example (1) In  $\mathbb{R}$ ,  $S_2$  above or  $[a, b] = \{z : a \leq z \leq b\}$

(2) In  $\mathbb{R}^2$ ,  $\{Q : \|PQ\| \leq r\}$

Interior point of  $S$ . Point  $P$  such that some neighbourhood of  $P$  consists entirely of points of  $S$ .

Open set A set in which every point is an interior point.



$C$  is closed.  $P$  is NR in  $C$ , i.e.  $P \in \bar{C}$   
Is it possible to find a neighbourhood  $P$   
consisting entirely of points in  $\bar{C}$ ?

Suppose this is not possible. Then, in  
any neighbourhood of  $P$ , there is a point  
not in  $\bar{C}$ , i.e. a point in  $C$ .

Then  $P$  is a limit point of  $C$ .  
But a closed set contains all its limit points.

$\therefore P \in C$ .

Contradiction.

$\therefore$  Every point of  $\bar{C}$  can be lies in  
neighbourhood of points of  $\bar{C}$ .

$\therefore$  Every point is an interior point.

$\therefore \bar{C}$  is an open set.

Complement of an open set.

$\Omega$  open set. We want to show that any limit point of  $\bar{\Omega}$  is in  $\bar{\Omega}$ . (R.I.P.)

If  $P$  is a limit point of  $\bar{\Omega}$ , any neighbourhood of  $P$  contains points of  $\bar{\Omega}$ , not  $P$ .

We want to show that  $P$  must be in  $\bar{\Omega}$ .

If this is not true  $P \notin \bar{\Omega}$ .

So some neighbourhood of  $P$  consists entirely of points of  $\bar{\Omega}$ .

i.e. it contains no points of  $\bar{\Omega}$ .

$\therefore P \in \bar{\Omega}$  only possible  
this.

So if  $P \notin \bar{\Omega}$ , it cannot be a limit point of  $\bar{\Omega}$ .

$\therefore$  All limit points of  $\bar{\Omega}$  are in  $\bar{\Omega}$ .

$\therefore$  Complement,  $\bar{\Omega}$ , of an open set is closed.

Union and intersection of open sets and of closed sets. 54

### Union of open sets $\cup O_r$

We expect this to be open. i.e. every part of  $\cup O_r$  should be an interior point of  $\cup O_r$ .

P is in  $\cup O_r$  if  $P \in O_i$  for some  $i$  in family  $\mathcal{O}_r$ .

- P is an interior point of  $O_i$ ,
- i.e. there is a neighbourhood P entirely in  $O_i$ .
- neighbourhood of P entirely in  $\cup O_r$ .
- $\therefore \cup O_r$  is open

### Intersection $\cap O_r$

Example.  $O_r = \{x : -\frac{1}{n} < x < \frac{1}{n}\}$ .

$$\bigcap_{n=1}^{\infty} O_r = \{0\} \quad 0 \text{ is not interior point.}$$

If could be open, if all  $O_r$  identical.

### Union of closed sets.

#### $\cup C_r$ .

$\{x : a \leq x \leq b\}$ . iff  $C_r = \{x : \frac{1}{n} \leq x \leq 1 - \frac{1}{n}\}$

$$\cup C_r = \{x : 0 < x < 1\} \text{ open}$$

$\bigcup_{n=2}^{\infty} C_r$  closed

If all  $C_r$  were identical,  $\cup C_r$  closed

### Intersection of closed sets $\cap C_r$ .

Suppose P is a limit point of  $\cap C_r$ .

Then any neighbourhood of P contains a point of  $\cap C_r$ .

A point is in  $\cap C_r$  if it is in every  $C_r$ .

$\therefore$  Any neighbourhood P contains a point of  $C_r$ .

$\therefore P$  is a limit point of  $C_r \therefore P \in C_r$ .

Similarly for every other  $C_r$ . i.e. for all  $C_r$

$\therefore P \in \cap C_r \therefore \cap C_r$  is closed

Complement of  $\cup_{\lambda r}$ .

If  $P$  is not in  $\cup_{\lambda r}$ .

$P \notin \lambda r$  for any  $r$ .

$\therefore P \in \bar{\lambda r}$  for each  $r$ .

$\therefore P \in \cap \bar{\lambda r}$ .

Complement of  $\cap_{\lambda r}$

$P$  is not in  $\cap_{\lambda r}$

$P$  is not in every  $\lambda r$

$\therefore P$  is not in some  $\lambda r$

$\therefore P \in \lambda r$  for some  $r$ .

$\therefore P \in \cup \bar{\lambda r}$

Intersection of closed sets.

$\cap G_r$ : if this is  $\cup \bar{G}_r$

$\bar{G}_r$  is open  
we should want  $\cap$  open is open

$\therefore \cup \bar{G}_r$  is open.

$\therefore$  its complement is closed.

$\therefore \cap G_r$  is closed.

## STIRLING APPROX TO $\nabla^2 V$

E ①  
56

$$\nabla^2 V.$$

$$\nabla^2 V = \operatorname{div} \operatorname{grad} V.$$

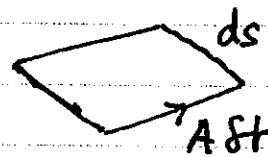
$$\text{If } V = V(x, y, z) \quad \operatorname{grad} V = \left( \frac{\partial V}{\partial x}, \frac{\partial V}{\partial y}, \frac{\partial V}{\partial z} \right)$$

The component of  $\operatorname{grad} V$  in any direction gives the rate of change of  $V$  in that direction. This is the space rate of change  $dV/ds$  where  $ds$  is the distance between the points in question.

It is important to notice this when co-ordinates other than  $(x, y, z)$  are used. e.g. in 2 dimensions, with polar co-ordinates the distances in  $r$  and  $\theta$  direction are  $dr, r d\theta$  so  $\operatorname{grad} V$  has components  $\frac{\partial V}{\partial r}, \frac{1}{r} \frac{\partial V}{\partial \theta}$

$$\text{Components } \frac{\partial V}{\partial r}, \frac{1}{r} \frac{\partial V}{\partial \theta}$$

flux  $A$ .  $A$  is defined at each point, and we interpret it as a velocity



In time  $\Delta t$ , any point within the parallelogram shown will cross the line element  $ds$ . The area of this parallelogram is  $A_n ds \Delta t$ , where  $A_n$  is the component of  $A$  along normal to  $ds$ . In 3-D, it will be a volume  $A_n dS \Delta t$ ,  $dS$  being an element of surface area. The rate at which areas or volumes are carried across a boundary is known as flux  $A$ . In 3-D, the vector  $dS$  is usually taken to mean a vector of magnitude  $dS$  in the direction of the normal. Thus rate at which volume crosses is  $A \cdot dS$ . For a surface it is  $\int A \cdot dS$ ,  $dS$  being outward normal in direction.

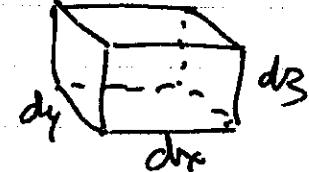
6 ②

$\text{div } A$  is the ratio of flux  $A$  out of some small region <sup>S/7</sup> to the volume of that region, as dimensions  $\rightarrow 0$ .

$$\text{If } A = (X, Y, Z)$$

The flux across ~~a face~~  
a face  $\perp OX$  is

$$X dy dz.$$



This flow will be into the box through left end, and out of box through right end. Thus net rate of loss is the difference between  $X dy dz$  taken at  $x + dx$  and taken at  $x$ .

The change in  $f(x, y, z)$  for such a displacement is  $\frac{\partial f}{\partial x} dx$ .

Thus faces  $\perp OX$  contribute  $dx \frac{\partial}{\partial x} (X dy dz)$ .

The dimensions  $dy, dz$  do not change, so we have  $\frac{\partial X}{\partial x} dx dy dz$ .

Applying same argument to faces  $\perp OY$  and faces  $\perp OZ$  we get

$$(\frac{\partial X}{\partial x} + \frac{\partial Y}{\partial y} + \frac{\partial Z}{\partial z}) dx dy dz \text{ as flux.}$$

$$\text{Flux per unit volume is } \frac{\partial X}{\partial x} + \frac{\partial Y}{\partial y} + \frac{\partial Z}{\partial z} = \text{div}(XYZ)$$

$$\text{If } (XYZ) = \text{grad } V, \quad X = \frac{\partial V}{\partial x}, \quad Y = \frac{\partial V}{\partial y}, \quad Z = \frac{\partial V}{\partial z}$$

$$\text{div grad } V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2}.$$

Note. When dealing with coordinates other than  $x, y, z$  care must be taken to consider areas of the faces.

Note however that for any coordinate

$$u, \quad \frac{df}{du} du \text{ gives } f(u+du) - f(u).$$

The question whether  $du$  is the same as  $ds$  does not arise. Only the definition of differentiation is involved.

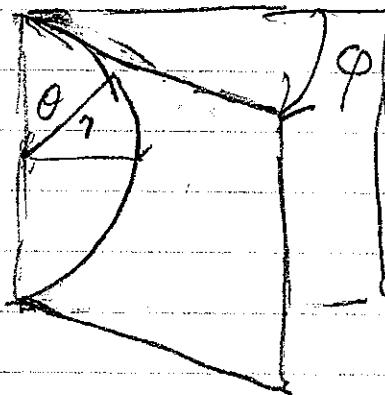
L (3)

58

### Spherical Polars.

To  $dr, d\theta, d\phi$  correspond distances,  $dr, r d\theta, r \sin \theta d\phi$ .

$$\text{Grad } V = \left( \frac{\partial V}{\partial r}, \frac{1}{r} \frac{\partial V}{\partial \theta}, \frac{1}{r \sin \theta} \frac{\partial V}{\partial \phi} \right)$$



$$r d\theta \quad r \sin \theta d\phi$$

For  $(A, B, C)$  flux through face 1  $dr$  is  $A r^2 \sin \theta d\theta d\phi$

$$\begin{aligned} \text{Net flux for faces 1 } dr & \text{ is } dr \frac{\partial}{\partial r} A r^2 \sin \theta d\theta d\phi \\ &= dr d\theta d\phi \frac{\partial}{\partial r} (A r^2 \sin \theta). \end{aligned}$$

$$\text{If } A = \frac{\partial V}{\partial r} \text{ this is } dr d\theta d\phi \frac{\partial}{\partial r} (r^2 \sin \theta \frac{\partial V}{\partial r}).$$

Flux through face 1  $d\theta$  is  $B r \sin \theta d\phi dr$ .

$$\begin{aligned} \text{Net flux is } d\theta \frac{\partial}{\partial \theta} (B r \sin \theta d\phi dr) \\ &= dr d\theta d\phi \frac{\partial}{\partial \theta} (B r \sin \theta) \end{aligned}$$

$$\text{If } B = \frac{1}{r} \frac{\partial V}{\partial \theta} \text{ this is } dr d\theta d\phi \frac{\partial}{\partial \theta} (\sin \theta \frac{\partial V}{\partial \theta})$$

Flux through face 1  $d\phi$  is  $C r d\theta dr$

$$\text{Net flux is } d\phi \frac{\partial}{\partial \phi} (C r d\theta dr) = dr d\theta d\phi r \frac{\partial}{\partial \phi} C$$

$$\text{If } C = \frac{1}{r \sin \theta} \frac{\partial V}{\partial \phi} \text{ this is } dr d\theta d\phi \frac{1}{\sin \theta} \frac{\partial^2 V}{\partial \phi^2}.$$

Volume of box is  $r^2 \sin \theta dr d\theta d\phi$ . Hence flux/volume

$$= \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial r} (r^2 \sin \theta \frac{\partial V}{\partial r}) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta \frac{\partial V}{\partial \theta}) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 V}{\partial \phi^2}$$

$$\text{So } \nabla \cdot V = \frac{1}{r^2} \frac{\partial}{\partial r} \left( \frac{r^2 \sin \theta}{r} \frac{\partial V}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial V}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 V}{\partial \phi^2}$$

L(k)

We now consider  $\nabla^2 V = FV$  where  $F$  may be 59 zero, a constant, or a function of  $r$  alone. These cases arise in various situations. In all cases  $F = F(r)$ .

Separation of Variables. We look for solutions of the form  $R(r)S(\theta, \phi)$ . We have

$$\frac{S}{r^2} \frac{d}{dr} \left( r^2 \frac{dR}{dr} \right) + \frac{R}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial S}{\partial \theta} \right) + \frac{R}{r^2 \sin^2 \theta} \frac{\partial^2 S}{\partial \phi^2} = F(r). RS$$

Multiply by  $\frac{r^2}{RS}$  and rearrange. This gives

$$\frac{1}{S \sin \theta} \left( \sin \theta \frac{\partial S}{\partial \theta} \right) + \frac{1}{S \sin^2 \theta} \frac{\partial^2 S}{\partial \phi^2} = r^2 F(r) - \frac{1}{R} \frac{d}{dr} \left( r^2 \frac{dR}{dr} \right)$$

L.H.S is  $f(\theta, \phi)$ : R.H.S is  $f(r)$ . They must both be constant, say  $k$ . Then, from L.H.S

$$\frac{1}{S \sin \theta} \left( \sin \theta \frac{\partial S}{\partial \theta} \right) + \frac{1}{S \sin^2 \theta} \frac{\partial^2 S}{\partial \phi^2} = k.$$

Multiply by  $\sin^2 \theta$  and look for  $S = \Theta(\theta) \Phi(\phi)$ . We find

$$\sin \theta \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial \Theta}{\partial \theta} \right) + \frac{1}{\Phi} \frac{d^2 \Phi}{d\phi^2} = k \sin^2 \theta$$

As before, this means  $\frac{1}{\Phi} \frac{d^2 \Phi}{d\phi^2}$  must be constant.

To give a satisfactory function this constant must be  $-m^2$ ,  $\frac{d^2 \Phi}{d\phi^2} = -m^2 \Phi$ .

Then  $\sin \theta \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial \Theta}{\partial \theta} \right) - (m^2 + k \sin^2 \theta) \Theta = 0$ .

$$\det \mu = \cos \theta \quad \frac{d\Theta}{d\mu} = \frac{d\Theta}{d\theta} / \frac{d\theta}{d\mu} = -\frac{1}{\sin \theta} \frac{d\Theta}{d\theta}$$

If  $\sin^2 \theta = 1 - \mu^2$  we have

$$(1 - \mu^2) \frac{d}{d\mu} \left[ (1 - \mu^2) \frac{d\Theta}{d\mu} \right] - (m^2 + k(1 - \mu^2)) \Theta = 0.$$

L(5)

S<sub>10</sub>

The singularities are at  $1, -1, \infty$ .

$$\text{Let } \mu_k = 1+t \quad 1-\mu^2 = -(2t+t^2)$$

$$(2t+t^2) \frac{d}{dt} (2t+t^2) \frac{d\Theta}{dt} - [m^2 + k(2t+t^2)]\Theta = 0$$

The lowest power terms are  $2t \frac{d}{dt} 2t \frac{d\Theta}{dt} - m^2 \Theta = 0$ .

$$\text{If } \Theta = t^\rho \quad 2t \frac{d\Theta}{dt} = \rho t^{\rho-1} \quad \therefore 4\rho^2 - m^2 = 0$$

$$\rho = \pm \frac{m}{2}. \quad \text{To stay finite we need } \rho = \frac{m}{2}$$

Similarly, or by symmetry,  $\rho > \frac{m}{2}$  for  $x = -1$ .

Thus we have  $(1-x^2)^{\frac{m}{2}}$ .  $d\Theta/dt = (1-x^2)^{\frac{m}{2}-1} z$ .

$$x \text{ for } \rho \quad \frac{d\Theta}{dx} = (1-x^2)^{\frac{m}{2}-1} z' - mx(1-x^2)^{\frac{m}{2}-2} z$$

$$(1-x^2) \frac{d\Theta}{dx} = (1-x^2)^{\frac{m}{2}+1} z' - mx(1-x^2)^{\frac{m}{2}} z$$

$$\begin{aligned} \frac{d}{dx} \left[ (1-x^2) \frac{d\Theta}{dx} \right] &= (1-x^2)^{\frac{m}{2}+1} z'' - (m+2)x(1-x^2)^{\frac{m}{2}} z' \\ &\quad - mx(1-x^2)^{\frac{m}{2}} z' - m(1-x^2)^{\frac{m}{2}} z^{\frac{m}{2}-1} \\ &\quad + m^2 x^2 (1-x^2)^{\frac{m}{2}-2} z \\ &= (1-x^2)^{\frac{m}{2}} z'' - (2m+2)x(2m+2)x(1-x^2)^{\frac{m}{2}} z' - \\ &\quad - m(1-x^2)^{\frac{m}{2}} z^{\frac{m}{2}-1} + m^2 x^2 (1-x^2)^{\frac{m}{2}-2} z? \end{aligned}$$

$$(1-x^2) \frac{d}{dx} \left( (1-x^2) \frac{d\Theta}{dx} \right) = (1-x^2)^{\frac{m}{2}+2} z'' - (2m+2)x(1-x^2)^{\frac{m}{2}+1} z' \\ = m(1-x^2)^{\frac{m}{2}+1} z^{\frac{m}{2}-1} + m^2 x^2 (1-x^2)^{\frac{m}{2}-2} z.$$

To this we add

$$-m^2(1-x^2)^{\frac{m}{2}} z^{\frac{m}{2}+1} + k(1-x^2)^{\frac{m}{2}} z.$$

Underlined terms combine to give

$$\underline{m^2(1-x^2)^{\frac{m}{2}} z^{\frac{m}{2}+1}} (x^2-1) = -m^2(1-x^2)^{\frac{m}{2}+1}$$

We may divide by  $(1-x^2)^{\frac{m}{2}+1}$  and obtain

$$(1-x^2)z'' - 2(m+1)xz' + z[m^2 - m^2 - m] = 0.$$

The solution has index 0 or  $x=1$  and  $x=-1$ ; unbranched.

From highest powers, if  $z \sim x^n$  for large  $x$

$$-N(N-1) - 2(m+1)N + k - n^2 - m^2 = 0$$

$$N^2 + N(2m+1) + n(n+1) - k = 0,$$

$$k = (N+m)(N+m+1)$$

$N$  must be natural number.

A special case is  $n=0$ . Then we can divide by  $(-x^2)$ . Replacing  $x$  by  $\alpha$  we have

$$\frac{d}{dx} \left( (-x^2) \frac{dy}{dx} \right) - ky = 0.$$

Singularities  $-1, 1, \infty$ .

Divergence method. Let  $x = 1+t$   $\frac{d}{dx} = \frac{dt}{dt}$

$$\frac{d}{dt} \left( 2t + t^2 \right) \frac{dy}{dt} + ky = 0.$$

$$(t^2 + 2t)y'' + (2 + 2t)y' + ky = 0.$$

Indicial equation, from  $2t y'' + 2y' \quad p(p-1) + p = 0 \quad p^2 = 0$ .

One soln has  $\ln t$ , and one is analytic at  $t=0$ .

Let  $y = \sum a_n t^n$  Coeff of  $t^{n+1}$  gives

$$0 = \cancel{\frac{1}{2}(n+1)n+2} \left[ 2n(n-1) + 2n \right] a_n + a_{n+1} \frac{(n-1)(n+2)+k}{2(n-1)+k}$$

$$0 = 2a_n n^2 + a_{n+1} [n^2 - n + k]$$

$$\frac{a_n}{a_{n+1}} = -\frac{1}{2} \left[ 1 - \frac{1}{n} + \frac{k}{n^2} \right]$$

$$\text{If } t = -2 \quad \frac{a_n t^n}{a_{n+1} t^{n+1}} = \frac{a_n}{a_{n+1}} t = 1 - \frac{1}{2} + \frac{k}{4}.$$

This diverges.  $\therefore$  Only way to get finite soln at 1 and  $-1$  is for the series to terminate.

If  $a_n t^n$  is higher power that occurs,  $a_{n+1} = 0$

$$\therefore (n+1)^2 - (n+1) + k = 0. \quad k = -n(n+1)$$

Berkely's method. An acceptable soln must be  $C_2$ -free at 1 and  $-1$ ,  $\therefore$  exponent 0 at each.  $\therefore$  Unbranched for circuit around infinity. From higher powers in original equation,

$$y'' \sim c x^n \text{ or } ((-x^2)y'' - 2xy' - ky = 0)$$

$$\text{From } x^2 y'' + 2xy' + ky \quad n(n-1) + 2n + k = 0 \quad k = -n(n+1).$$

This shows  $n$  must be integer.

$n$  must in fact be positive.

For central attraction in H atom  $V = -\frac{e^2}{r}$

$$T = \frac{1}{2m}(p_x^2 + p_y^2 + p_z^2) \quad T + V = E$$

$$p_x \rightarrow ik \frac{\partial}{\partial x}$$

$$-\frac{k^2}{2m} \left( \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} + \frac{\partial^2 \psi}{\partial z^2} \right) - \frac{e^2}{r} \psi = E \psi$$

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} + \frac{\partial^2 \psi}{\partial z^2} + \frac{2m(E + \frac{e^2}{r})}{k^2} \psi = 0$$

$$\text{Thus } \nabla^2 V + (a + \frac{b}{r}) \psi = 0.$$

Spherical polar co-ordinates

Distances  $dr, r d\theta, r \sin \theta d\phi$

$$\therefore \text{grad } \psi = \left( \frac{\partial \psi}{\partial r}, \frac{1}{r} \frac{\partial \psi}{\partial \theta}, \frac{1}{r \sin \theta} \frac{\partial \psi}{\partial \phi} \right)$$



The areas of faces are

$$L_r \quad r^2 \sin \theta \, dr \, d\theta \, d\phi$$

$$L_\theta \quad r \sin \theta \, dr \, d\phi$$

$$L_\phi \quad r \, dr \, d\theta$$

For vector  $\underline{A} = (A_r, A_\theta, A_\phi)$

$$\begin{aligned} \text{div. } \underline{A} &= \frac{\partial}{\partial r} \left( r^2 \sin \theta \frac{\partial A_r}{\partial r} \right) + \frac{\partial}{\partial \theta} \left( A_\theta r \sin \theta \frac{\partial A_r}{\partial \theta} \right) \\ &\quad + \frac{\partial}{\partial \phi} \left( A_\phi r \sin \theta \frac{\partial A_r}{\partial \phi} \right) \end{aligned}$$

$$r^2 \sin \theta \, dr \, d\theta \, d\phi$$

$$= \frac{1}{r^2 \sin \theta} \left[ \frac{\partial}{\partial r} (r^2 \sin \theta A_r) + \frac{\partial}{\partial \theta} (A_\theta r \sin \theta) + \frac{\partial}{\partial \phi} (A_\phi r) \right]$$

Putting  $A = \text{grad } \psi$

$$\begin{aligned} \nabla^2 \psi &= \frac{1}{r^2 \sin \theta} \left[ \frac{\partial}{\partial r} (r^2 \sin \theta \frac{\partial \psi}{\partial r}) + \frac{\partial}{\partial \theta} (\sin \theta \frac{\partial \psi}{\partial \theta}) + \frac{\partial}{\partial \phi} (\frac{1}{r \sin \theta} \frac{\partial \psi}{\partial \phi}) \right] \\ &= \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 \frac{\partial \psi}{\partial r}) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta \frac{\partial \psi}{\partial \theta}) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 \psi}{\partial \phi^2} \end{aligned}$$

So we have

$$\frac{1}{r^2} \frac{\partial}{\partial r} (r^2 \frac{\partial \psi}{\partial r}) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta \frac{\partial \psi}{\partial \theta}) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 \psi}{\partial \phi^2} + (a + \frac{b}{r}) \psi = 0$$

Let  $\psi = RS \quad R(r) \leq (\theta, \varphi)$

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$$\frac{S}{r^2} \frac{d}{dr} \left( r^2 \frac{dR}{dr} \right) + \frac{R}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial S}{\partial \theta} \right) + \frac{R}{r^2 \sin^2 \theta} \frac{\partial^2 S}{\partial \varphi^2} +$$
$$(a + \frac{b}{r}) RS = 0.$$

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$$\div RS \times r^2$$

$$\frac{1}{R} \frac{d}{dr} \left( r^2 \frac{dR}{dr} \right) + \left( a + \frac{b}{r} \right) r^2 +$$
$$+ S \frac{1}{\sin \theta} \frac{d}{d\theta} \left( \sin \theta \frac{\partial S}{\partial \theta} \right) + \frac{1}{S \sin^2 \theta} \frac{\partial^2 S}{\partial \varphi^2} = 0.$$

Each part must be constant.

$$\frac{d}{dr} \left( r^2 \frac{dR}{dr} \right) + (ar^2 + br + d) R = 0$$

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NUMBER	APPROXIMATION	FACTORIAL	RATIO
1	0.922137009	1	1.08443755
2	1.91900435	2	1.04220712
3	5.83620959	6	1.02806452
4	23.5061751	24	1.0210083
5	118.019168	120	1.01678399
6	710.078185	720	1.01397285
7	4980.39583	5040	1.01196776
8	39902.3955	40320	1.01046565
9	359536.873	362880	1.00929843
10	3598695.62	3628800	1.00836536
11	39615625	39916800	1.00760243
12	475687486	479001600	1.006967
13	6.18723948E9	6.2270208E9	1.00642958
14	8.66610018E10	8.71782912E10	1.00596911
15	1.30043072E12	1.30767437E12	1.00557019
16	2.08141144E13	2.09227899E13	1.00522124
17	3.53948329E14	3.55687428E14	1.00491343
18	6.37280462E15	6.40237371E15	1.00463989
19	1.21112787E17	1.216451E17	1.00439519
20	2.42278685E18	2.43290201E18	1.00417501
21	5.08886173E19	5.10909422E19	1.00397584
22	1.11975149E21	1.12400073E21	1.0037948
23	2.57585254E22	2.58520167E22	1.00362953
24	6.18297927E23	6.20448402E23	1.00347806
25	1.54595948E25	1.55112101E25	1.00333872
26	4.02000993E26	4.03291461E26	1.00321011

TIME

75.44

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*S<sub>15</sub>*

BERNOULLI NUMBERS

B(0)=1  
B(1)=-0.5  
B(2)=0.166666667  
B(3)=0  
B(4)=-0.033333334  
B(5)=0  
B(6)=0.0238095245  
B(7)=0  
B(8)=-0.0333333379  
B(9)=0  
B(10)=0.0757576189  
B(11)=0  
B(12)=-0.253114136  
B(13)=0  
B(14)=1.16667745  
B(15)=0  
B(16)=-7.09241926  
B(17)=0  
B(18)=54.979315  
B(19)=0  
B(20)=-529.43755  
B(21)=0  
B(22)=6206.78938  
B(23)=0  
B(24)=-87400.5253  
B(25)=0  
B(26)=1479539.33  
B(27)=0  
B(28)=-31436265.9  
B(29)=0  
B(30)=966346303  
B(31)=0  
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Bernoulli's numbers.

$$\frac{x}{e^x - 1} = B_0 + \frac{B_1}{1!} x + \frac{B_2}{2!} x^2 + \dots + \frac{B_n}{n!} x^n + \dots$$

$$\text{LHS} = \frac{1}{\frac{1}{1!} + \frac{x}{2!} + \frac{x^2}{3!} + \frac{x^3}{4!} + \dots}$$

$$\text{so } 1 = \left( \frac{1}{1!} + \frac{x}{2!} + \frac{x^2}{3!} + \dots \right) \left( B_0 + \frac{B_1}{1!} x + \frac{B_2}{2!} x^2 + \dots \right)$$

$$B_0 = 1$$

$$0 = \frac{1}{2!} \frac{B_0}{0!} + \frac{1}{1!} \frac{B_1}{1!}$$

In general

$$\text{Coef } x^n = \frac{1}{n!} \frac{B_0}{0!} + \frac{1}{(n-1)!} \frac{B_1}{1!} + \frac{1}{(n-2)!} \frac{B_2}{2!} + \dots + \frac{1}{1!} \frac{B_{n-1}}{(n-1)!} = 0$$

$$\text{Multiply by } \binom{n}{0} B_0 + \binom{n}{1} B_1 + \binom{n}{2} B_2 + \dots + \binom{n}{n-1} B_{n-1} = 0$$

(interesting special symbols.)

$$\text{indices to subscripts - } B_0 = 1 \quad (0)$$

$$\text{Thus } B_1 = 0 \quad (1)$$

$$2B_2 + 1 = 0 \quad (2)$$

$$3B_3 + 3B_1 + 1 = 0 \quad (3)$$

$$3B_2 + 6B_2 + 4B_1 + 1 = 0 \quad (4) \text{ etc.}$$

$$4B_4 + 10B_3 + 10B_2 + 5B_1 + 1 = 0 \quad (5)$$

$$5B_5 + 10B_4 + 10B_3 + 5B_2 + B_1 = 0 \quad (6)$$

If turns out that  $B_1 = -\frac{1}{2}$   $B_3 = B_5 = B_7 = \dots = 0$

This suggests that  $L.H.S + \frac{1}{2}x$  is an even function.

$$\text{LHS} + \frac{1}{2}x = \frac{x}{e^x - 1} + \frac{1}{2}x = x \left\{ \frac{1}{e^x - 1} + \frac{1}{2} \right\}$$

$$= x \left\{ \frac{1 + \frac{1}{2}(e^x - 1)}{e^x - 1} \right\} = \frac{x}{2} \frac{e^x + 1}{e^x - 1}$$

$$\text{Replacing } x \text{ by } -x \text{ gets } -\frac{x}{2} \frac{e^{-x} + 1}{e^{-x} - 1} = -\frac{x}{2} \frac{1 + e^x}{1 - e^x}$$

$$= \frac{x}{2} \frac{e^x + 1}{e^x - 1} \text{ so all odd coeffs, after } B_1, \text{ are zero.}$$

$B_2, B_4, B_6, \dots$  can be calculated by recursion from equations above.  $B_2$  from (2),

$B_4$  from 4 and so on.

## BERNOULLI NUMBERS

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B(28)=-31436265.9  
B(29)=0  
B(30)=966346303  
B(31)=0  
>

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$N$	$\sqrt{2\pi n}^n n^{-n}$	$n!$	Ratio	S18
1	.922 137009	1	1.0844	
2	1.919 004 351	2	1.0422	
3	5.836 209 590	6	1.028 064 578	
4	23.506 175 14	24	1.021 008 303	
5	118.019 167 9	120	1.016 783 986	
6	710.078 184 7	720	1.013 972 849	
7	4980. 395 833	5040	1.011 967 757	
8	39,902. 395 44	40,320	1.010 465 651	
9	359,536. 8729	362,880	1.009 298 426	
10	3,598,695.619	3,628,800	1.008 365 359	
11	39,615,625.66	39,946,800	1.007 602 428	
12	475,687,486.4	479,001,600	1.006 966 856	
13	6,187,239,477	6,227,020,800	1.006 429 575	

$$20 \quad 2.422 786.8 \times 10^{18} \quad 2.422 9020 \times 10^{18} \quad 1.006 175010$$

Asymptotic series.

Knopp (p 521) gives example: if we can prove

$$(I) f(x) = 1 - \frac{1!}{x} + \frac{2!}{x^2} - \frac{3!}{x^3} + \cdots + (-1)^n \frac{n!}{x^n} + (-1)^{n+1} \frac{(n+1)!}{x^{n+1}}$$

$0 < x < 1.$

The infinite series  $\sum_0^\infty (-1)^n \frac{n!}{x^n}$  is divergent for all  $x$ , since terms increase in magnitude for  $n > x$ .

However, since the form of the remainder is known we can calculate  $f(1000)$  to about 10 decimal places with ease.

$$\text{For } n=3 \quad \frac{(n+1)!}{1000^{n+1}} = \frac{4!}{10^{12}} = .000\ 000\ 000\ 024$$

The error due to taking  $f(x) = 1 - \frac{1}{x} + \frac{2}{x^2} - \frac{6}{x^3}$  and  $x = 1000$  is less than  $.000\ 000\ 000\ 1$ .

For any  $x$ , the terms decrease in magnitude

for  $n < x$ , increase for  $n > x$ .  
The error above is  $\sqrt[n+1]{T_{n+1}}$ , where  $T_{n+1}$  is term in  $\frac{1}{x^{n+1}}$ .

This is a minimum term for each  $x$ .  
The error cannot be made arbitrarily less than this minimum by using the series.

We can always say, if we consider only terms up to  $T_n$ , that result is an error less than  $\sqrt[n+1]{T_{n+1}}$ , the first term omitted.

This property is possessed by a series like

$$1 - \frac{1}{2} + \frac{1}{3} - \frac{1}{4} + \frac{1}{5} - \frac{1}{6} \quad -\int \int \int \int \dots$$

Series (I) has the same property, but of course for quite different reasons.

Stirling's asymptotic series for  $\ln n!$

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$$\ln n! \approx (n+\frac{1}{2})\ln n - n + (\sqrt{2\pi} +$$

S

$$+ \frac{B_2}{1 \cdot 2} \frac{1}{n} + \frac{B_4}{3 \cdot 4} \frac{1}{n^3} + \frac{B_6}{5 \cdot 6} \frac{1}{n^5} + \dots + \frac{B_{2k}}{(2k-1)2k} \frac{1}{n^{2k-1}} \dots$$

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This series does not converge for any value of  $n$ ; this is reasonable in view of the way the coefficients  $B_{2k}$  increase.

Yet it has the property that the error made in stopping at any number of terms is numerically less than the first term omitted, and of course

$$B_2 = \frac{1}{6}, \quad B_4 = -\frac{1}{360}.$$

Thus error in stopping at  $\sqrt{2\pi}$  is less than

$\frac{1}{12n}$ ; the estimate is too small.

If we stopped at  $\frac{B_2}{1 \cdot 2} \frac{1}{n}$  the error is less than

As  $B_4$  is negative,

$$\left| \frac{B_4}{3 \cdot 4} \frac{1}{n^3} \right| = \frac{1}{360n^3}$$

The estimate is now too large.

So we should add less than  $\frac{1}{12n}$  but

$$\text{more than } \frac{1}{12n} - \frac{1}{360n^3}.$$

For  $n=1$ ,  $n!=1$ ,  $n!\text{estimated} = 0.922137007$

Logarithms, 0 and  $-0.08106\dots$

$$\frac{1}{12} = 0.083 \quad \frac{1}{12} - \frac{1}{360} = 0.0805$$

6 ①

Jeffreys and Jeffreys. § 9.08.

Euler-Maclaurin formula.  $f$  differentiable. Integrate by parts, twice

$$\begin{aligned}
 \int_0^1 f(x) dx &= \left[ x f(x) \right]_0^1 - \int_0^1 x f'(x) dx \\
 &= f(1) - \int_0^1 x f'(x) dx \\
 &= f(1) - \int_0^1 (x - \frac{1}{2}) f'(\bar{x}) d\bar{x} - \int_0^1 \frac{1}{2} f''(\bar{x}) d\bar{x} \\
 &= f(1) - \frac{1}{2} f(1) + \frac{1}{2} f(0) - \int_0^1 (x - \frac{1}{2}) f''(\bar{x}) d\bar{x} \\
 &= \frac{1}{2} f(1) + \frac{1}{2} f(0) - \int_0^1 (x - \frac{1}{2}) f''(\bar{x}) d\bar{x}.
 \end{aligned}$$

Trapezoidal rule with integral is correct.  
For  $0 \leq x \leq 1$  and  $r \geq 2$  define

$\forall r \quad P_r(0) = 0$

$P_2'(x) = x - \frac{1}{2} \quad (2)$

$P_3'(x) = b_2 + P_2(x) \quad (3)$

$P_4'(x) = b_3 + P_3(x) \quad (4)$

$\bar{P}_r'(x) = \bar{b}_{r-1} + \bar{P}_{r-1}(x)$

Choose  $b_r$  so that  $P_r(1) = 0$  for all  $r \geq 2$ .

Then  $P_r(x) = \int_0^x \bar{b}_{r-1} + \bar{P}_{r-1}(\bar{s}) ds$

$P_r(1) = 0$  means  $\bar{P}_{r-1}(0) = \int_0^1 \bar{b}_{r-1} + \bar{P}_{r-1}(\bar{s}) ds$

i.e.  $\bar{b}_{r-1} = - \int_0^1 \bar{P}_{r-1}(\bar{s}) ds$ .

$r \rightarrow r+1 \quad b_r = - \int_0^r \bar{P}_r(\bar{s}) ds$

Keep interpretation by parts

$\int_0^1 P_2'(x) f'(x) dx = \left[ P_2(x) f''(x) \right]_0^1 - \int_0^1 P_2(x) f'''(x) dx$

$= - \int_0^1 P_2(x) f'''(x) dx$

$= - \left( \left\{ P_3'(\bar{x}) - b_2 \right\} f''(\bar{x}) \right) \text{ by } (2)(3)$

$= - b_2 \left[ f'(\bar{x}) \right]_0^1 - \left[ P_3(x) f''(x) \right]_0^1 + \int_0^1 P_3(x) f'''(x) dx$

$$\begin{aligned}
 &= b_2 \{ f'(1) - f'(0) \} + \int_0^1 P_3(x) f'''(x) dx \quad 7(2) \\
 &= b_2 \{ f'(1) - f'(0) \} + \int_0^1 (P_4'(x) - b_3) f''(x) dx \quad h(x)(4) \\
 &= b_2 \{ f'(1) - f'(0) \} - b_3 \{ f''(1) - f''(0) \} + \int_0^1 P_4'(x) f''(x) dx \\
 &= b_2 \{ f'(1) - f'(0) \} - b_3 \{ f''(1) - f''(0) \} + [P_4(x) f''(x)]_0^1 \\
 &\quad - \int_0^1 P_4(x) f'''(x) dx \\
 &- \int_0^1 P_4(x) f'''(x) dx = - \int_0^1 (P_5'(x) - b_4) f''''(x) dx \quad h(x)(5) \\
 &\int_0^1 b_4 f''''(x) dx = b_4 \{ f''''(1) - f''''(0) \} \\
 &- \int_0^1 P_5'(x) f''''(x) dx = - [P_5(x) f''''(x)]_0^1 + \int_0^1 P_5(x) f''''(x) dx \\
 &= \int_0^1 P_5(x) f''''(x) dx.
 \end{aligned}$$

Thus

$$\int_0^1 P_n'(x) f'(x) dx = \sum_{r=2}^n (-1)^r \{ f^{(r)}(1) - f^{(r-1)}(0) \} - (-1)^n \int_0^1 P_{n+1}'(x) f''(x) dx$$

Stages:

$$\begin{aligned}
 \text{rat } 2: \int_0^1 P_2'(x) f'(x) dx &= b_2 \{ f'(1) - f'(0) \} - \int_0^1 P_3'(x) f''(x) dx \\
 \text{rat } 3: \int_0^1 P_2'(x) f'(x) dx &= b_2 \{ f'(1) - f'(0) \} - b_3 \{ f''(1) - f''(0) \} + \\
 &\quad + \int_0^1 P_4'(x) f'''(x) dx \\
 \text{rat } 4: \int_0^1 P_2'(x) f'(x) dx &= b_2 \{ f'(1) - f'(0) \} - b_3 \{ f''(1) - f''(0) \} + \\
 &\quad + b_4 \{ f'''(1) - f'''(0) \} - \int_0^1 P_5'(x) f^{(iv)}(x) dx.
 \end{aligned}$$

in agreement with Jeffreys & Jeffreys.

Now consider the series  $\frac{a}{e^a - 1} + \frac{1}{2} a = \sum_{n=0}^{\infty} b_n a^n$  (6)

$$a \frac{e^{ar} - 1}{e^a - 1} = \sum_{r=0}^{\infty} P_r(t) a^r. \quad (7)$$

The  $\{b_n\}$ ,  $\{P_r(t)\}$  so defined are identical with those used above.

$$\begin{aligned}
 \frac{\partial}{\partial t} a \frac{e^{ar}}{e^a - 1} &= a \frac{ae^{ar}(e^a - 1) / e^a (e^a - 1)}{(e^a - 1)^2} \\
 &= \frac{a^2 (e^{ar} - 1)}{e^a - 1} \quad \text{a const!}
 \end{aligned}$$

$$\begin{aligned}
 \frac{a^2 e^{ar}}{e^a - 1} &= \frac{a^2 (e^{ar} - 1)}{e^a - 1} + \frac{a^2}{e^a - 1} \\
 &= \sum_{r=0}^{\infty} P_r(t) a^{r+1} + a \left\{ \sum_{n=0}^{\infty} b_n a^n - \frac{1}{2} a^2 \right\}
 \end{aligned}$$

$$\text{Thus } = \sum_{r=0}^{\infty} P_r'(t) a^r. \quad \text{equals left of } a^n$$

$$P_r'(t) = P_{r-1}(t) + \frac{b_{r-1}}{a^n} \quad \text{exactly as (2)(7).}$$

See over

All conditions are satisfied.

Notes on T & S derivation of Euler-Maclaurin. 9

$f$  differentiable. (means "f analytic")

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$$\int_0^1 f(x) dx = [x f(x)]_0^1 - \int_0^1 x f'(x) dx \\ = \frac{1}{2} f(1) + \frac{1}{2} f(0) - \int_0^1 (x - \frac{1}{2}) f''(x) dx \quad [17]$$

correction of Trapezoidal rule.

Sequence of polynomials defined by

If  $P_r(0) = 0$ . If  $P_r(1) = 1$  fixed b

$$P_2'(x) = x - \frac{1}{2} \quad (2)$$

$$P_2'(x) = b_{r-1} + P_{r-1}(x) \quad (1)$$

$$P_2'(x) = x - \frac{1}{2} \quad P_2'(x) = \frac{1}{2}x^2 - \frac{1}{2}x + c. \\ \text{and } c=0 \text{ so } P_2(x) = \frac{1}{2}x^2 - \frac{1}{2}x$$

$$P_3'(x) = b_2 + P_2(x)$$

$$P_2(1) - P_3(0) = \int_0^1 P_3'(x) dx = b_2 + \int_0^1 P_2(x) dx \\ \therefore b_2 = - \int_0^1 P_2(x) dx = - \left[ \frac{1}{6}x^3 - \frac{1}{4}x^2 \right]_0^1 \\ - \left[ \frac{1}{6} - \frac{1}{4} \right] = -\frac{1}{12}$$

$$B_2 = \frac{1}{6} = 2! b_2.$$

$$\text{Generally } b_r = - \int_0^1 P_r(x) dx.$$

We have  $\int_0^1 (x - \frac{1}{2}) f'(x) dx$  as starting point

$$= \int_0^1 P_2'(x) f'(x) dx = [P_2(x) f'(x)]_0^1 - \int_0^1 P_2(x) f''(x) dx$$

$P_2(x)$  zero at both end of [ ].

$$\text{So } + \int_0^1 P_2(x) f''(x) dx = \text{last term on [1]}$$

$$= \left( \int_0^1 P_3'(x) - b_2 \cdot \cancel{f''(x)} dx \right)$$

$$= \left[ -b_2 f'(x) \right]_0^1 + \int_0^1 P_3(x) f''(x) dx - \int_0^1 P_3(x) f''' dx \\ \text{zero.}$$

$$= -b_2 (f'(1) - f'(0)) - \int_0^1 P_3(x) f''' dx$$

We have a term  $-\int_0^1 P_3(x) f''' dx$

Note 2

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S

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$$= \int_0^1 \{b_3 - P_4'(x)\} f''' dx$$

$$= b_3 \{f'''(1) - f'''(0)\} - \int_0^1 P_4'(x) f''' dx$$

$b_3$  term has + sign, but  $b_3 = 0$

$$\underline{-\int_0^1 P_4'(x) f''' dx = -[P_4(x) f'''(x)]_0^1 + \int_0^1 P_4(x) f'''' dx}$$

$$+ \int_0^1 P_4(x) f''''(x) dx = \int_0^1 (P_5'(x) - b_4) f'''' dx$$

$$= -b_4 [f''''(1) - f''''(0)] \text{ with } \int_0^1 P_5'(x) f'''' dx$$

$$\text{Integral} = \underline{\{P_5(x) f'''\}}_0^1 - \int_0^1 P_5(x) f''' dx$$

$$= - \int_0^1 P_5(x) f''' dx$$

Compare this with  $-\int_0^1 P_3(x) f''' dx$  above.

Also compare  $+ \int_0^1 P_4(x) f''''(x) dx$

with  $+ \int_0^1 P_2(x) f''''(x) dx$  earlier.

J&J. p465

$$3! = \lim_{n \rightarrow \infty} \frac{n! \cdot n^3}{(3+1)(3+2) \cdots (3+n)} \quad R(3) > -1. \quad 11$$

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$$\ln 3! = \lim \left\{ \ln n! + 3 \ln n - \sum_{i=1}^n \frac{1}{3+i} \right\}$$
$$F(3) = \frac{d}{d_3} \ln 3! = \lim \left\{ \ln n - \frac{1}{3+i} \right\}$$
$$F'(3) = \frac{d^2}{d_3^2} \ln 3! = \ln \sum_{i=1}^{\infty} \frac{1}{(3+i)^2}$$
$$= \sum_{i=1}^{\infty} \frac{1}{(3+i)^2}$$

p 466 § 15-05

$$\int_0^\infty \frac{dx}{(3+x)^2} = \left[ -\frac{1}{3+x} \right]_0^\infty = \frac{1}{8}.$$

Euler Maclaurin.

$$\int_0^n f(x) dx = \frac{1}{2} f(0) + f(1) + f(2) + \dots + f(n)$$
$$- b_2 \{ f(n) - f'(0) \} - b_4 \{ f''(n) - f''(0) \} - \dots$$
$$- b_{2r} \{ f^{(2r-1)}(n) - f^{(2r-1)}(0) \} -$$
$$- \sum_{m=0}^{n-1} \int_m^{m+1} P_{2r+1}(x-m) f^{(2r+1)}(x) dx.$$

Applying this to  $f(x) = 1/(3+x)^n$ ,  $n \rightarrow \infty$ .

$$F'(3) = \frac{1}{8} - \frac{1}{2 \cdot 8^2} + \frac{B_2}{3^3} + \frac{B_4}{2^5} + \frac{B_{2r}}{8^{2r+1}} +$$

$$+ \sum_{m=0}^{\infty} \int_m^{m+1} \frac{(2r+2) \phi_{2r+1}(x-m)}{(3+x)^{2r+3}} dx$$

where  $\phi_r(x) = r! P_r(x)$  (p. 280)

? remark under  
eqn (2) p 466.

$$F(3) = \ln 3 + \frac{1}{2 \cdot 8} - \frac{B_2}{2 \cdot 8^2} - \frac{B_4}{4 \cdot 8^4} - \frac{B_{2r}}{2r \cdot 8^{2r}} - \sum_{m=0}^{\infty} \int_m^{\infty} \frac{\phi_{2r+1}(x-m)}{(3+x)^{2r+2}} dx$$

$$\therefore \ln 3! = C + (3+\frac{1}{2}) \ln 3 - 3 + \frac{B_2}{2 \cdot 3} + \frac{B_4}{3 \cdot 4 \cdot 3^3} + \dots \quad (4)$$

in the sense that  $\ln 3!$  lie between sum of terms  
and  $(r+1)$  terms of the series.

$C$  has to be found. Take  $z$  large, and use 12

$$z! (z-\frac{1}{2})! = 2^{-2z} \sqrt{\pi} (2z)! \approx \text{the form } \frac{5}{27}$$

$$\ln z! + \ln (z-\frac{1}{2})! = -2z \ln 2 + \frac{1}{2} \ln \pi + \ln (2z)!$$

Substitute from (4). The terms that do not tend to zero give

$$C + (z+\frac{1}{2}) \ln z_n^3 + C + \ln z \ln (z-\frac{1}{2}) - (z-\frac{1}{2}) \\ = -2z \ln 2 + \frac{1}{2} \ln \pi + C + (2z+1) \ln 2z - (2z)$$

$$C + \underline{(z+\frac{1}{2}) \ln z} + 3 \ln (z-\frac{1}{2}) - 2z + \frac{1}{2} \\ = \underline{-2z \ln 2} + \frac{1}{2} \ln \pi + \underline{(2z+1) \ln 2} + \\ + \ln 2$$

$$\text{LHS: } C - (z+\frac{1}{2}) \ln z + 3 \ln (z-\frac{1}{2}) - 2z + \frac{1}{2} \\ 3 \ln (z-\frac{1}{2}) = 3(\ln z + \ln(1-\frac{1}{2z})) \\ \approx 3 \ln z - \frac{1}{2}$$

$B_{2n}$  alternate in sign.

$$\varphi_2(x) = x^2 - x$$

$$\varphi_3(x) = x^3 - \frac{3}{2}x^2 + \frac{1}{2}x$$

$$= x(x-1)(x-\frac{1}{2})$$

$$\varphi_4(x) = x^4 - 2x^3 + x^2$$

$$= x^2(x-1)^2$$

$$\varphi_5(x) = x^5 - \frac{5}{2}x^4 + \frac{5}{3}x^3 - \frac{1}{6}x$$

$\varphi_n(0) = 0$   $\varphi_n(1) = 0$   
by definition.

s  
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Structure of  $J$  &  $J'$  Euler MacLaurin Theorem.

p 278 By successive integration by parts 29

$$\int_0^1 P_2'(x) f'(x) dx = b_2 \{ f'(1) - f'(0) \} + -b_3 \{ ? + \dots + (-1)^n b_n \{ f^{(n-1)}(1) - f^{(n-1)}(0) \} - (-1)^n \int_0^1 P_{n+1}(x) f^{(n+1)}(x) dx \}$$

$$\begin{aligned} \int_0^1 P_2'(x) f'(x) dx &= \int_0^1 (x - \frac{1}{2}) f'(x) dx \\ &= \frac{1}{2} f(0) + \frac{1}{2} f(1) - \int_0^1 f(x) dx \end{aligned}$$

Apply this result to intervals  $(0,1), (1,2) \dots (n-1, n)$

in turn and add

$$\begin{aligned} \text{We get } \int_0^n f(x) dx &= \frac{1}{2} f(0) + f(1) + \dots + f(n-1) + \frac{1}{2} f(n) \\ &\quad - b_2 \{ f'(n) - f'(0) \} - b_3 \{ f''(n) - f''(0) \} \\ &\quad \dots - b_{2r} \{ f^{(2r-1)}(n) - f^{(2r-1)}(0) \} \\ &\quad - \sum_{m=0}^{2r} \int_m^{m+1} P_{2r+1}(x-m) f^{(2r+1)}(x) dx \\ &\quad \text{Top of p 281. Why error less than neglected term.} \end{aligned}$$

$$\varphi_2(x) = x^2 - x$$

$$(\frac{1}{2}+t)(-\frac{1}{2}+t) = t^2 - \frac{1}{4}$$

$$\varphi_3(x) = x^3 - \frac{3}{2}x^2 + \frac{1}{2}x$$

$$\varphi_4(x) = x^4 - 2x^3 + x^2$$

$$x = t + \frac{1}{2} \quad \varphi_2(x) = t^2 + \frac{1}{4}t + \frac{1}{4} = t^2 - \frac{1}{4}$$

$$\begin{aligned}\varphi_3(x) &= t^3 + \frac{3}{2}t^2 + \frac{3}{4}t + \frac{1}{8} \\ &\quad - \frac{3}{2}t^2 - \frac{3}{2}t + \frac{3}{8} \\ &\quad + \frac{5}{4}t + \frac{1}{4} \\ &= \underline{t^3 - \frac{1}{4}t}\end{aligned}$$

$$P_2 = \frac{1}{2}t^2 - \frac{1}{8}$$

$$\begin{aligned}P_2' &= 2t \\ P_3' &= 3t^2 - \frac{1}{4}\end{aligned}$$

$$\begin{aligned}P_2' &= t \\ P_3' &= \frac{\varphi_3'}{6} = \frac{t^2}{2} - \frac{1}{24}\end{aligned}$$

$$\begin{aligned}&= P_2 + \frac{1}{8} - \frac{1}{24} \\ &= P_2 + \frac{3-1}{24} = P_2 + \frac{1}{12}\end{aligned}$$

$$P_3' = b_2 + \frac{1}{2}t^2 - \frac{1}{8}$$

$$P_3 = \frac{1}{6}(t^3 - 1)$$

$$P_3 = \frac{1}{6}t^3 + t(b_2 - \frac{1}{8}) + c$$

$$P_3(0) = 0 \quad \therefore c = 0 \quad \frac{1}{6} + b_2 - \frac{1}{8} = 0 \quad b_2 = \frac{1}{8} - \frac{1}{6}$$

$$P_3(1) = 0 \quad \therefore \quad = -$$

$$P_4' = b_3 + \frac{1}{6}(t^3 - 1)$$

$P_4$  wec<sup>n</sup> even

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$$P_n(x) = \varphi_r(x)/n!$$

$$\varphi_2(x) = x^2 - x \quad \varphi_2\left(\frac{t}{2}\right) = -\frac{1}{4}$$

$$1, \frac{1}{6}, \frac{4}{15}, \frac{10}{20}, \frac{10}{15}, \frac{4}{5}, \frac{1}{6}, \frac{1}{1} \\ \varphi_4(x) = [x(x-1)]^2 \quad \varphi_4\left(\frac{t}{2}\right) = \left[\frac{t}{2}(t-\frac{1}{2})\right]^2 = \frac{1}{16}$$

$$\varphi_6(x) = x^6 - 3x^5 + \frac{5}{2}x^4 - \frac{1}{2}x^2$$

$$\varphi_6\left(\frac{t}{2}\right) = \frac{1}{64} - \frac{3}{32} + \frac{5}{32} - \frac{1}{8} = \frac{1}{64} + \frac{1}{16} - \frac{1}{8} = \frac{1+4-8}{64}$$

$$\begin{aligned} \varphi_6(1-t) &= (1-t)^6 - 3(1-t)^5 + \frac{5}{2}(1-t)^4 - \frac{1}{2}(1-t)^2 \\ &= 1 - 6t + 15t^2 - 20t^3 + 15t^4 - 6t^5 + t^6 \\ &\quad - 3 - 15t - 30t^2 + 30t^3 - 15t^4 + 3t^5 \\ &\quad + \frac{5}{2} - 10t + 15t^2 - 10t^3 + \frac{5}{2}t^4 \\ &\quad - \frac{1}{2} + t - \frac{1}{2}t^2 \\ &\quad \underline{- \frac{1}{2}t^2} \quad \underline{+ \frac{5}{2}t^4} - 3t^5 + t^6. \end{aligned}$$

$$\varphi_6(1-t) = \varphi_6(t)$$

$$\underline{\varphi_6'(1-t) = 1-t - \frac{1}{2} = \frac{1}{2} - t = -P_2'(t)}$$

$$P_2'(1-t) = 1-t - \frac{1}{2} = \frac{1}{2} - t = -P_2'(t)$$

$$P_3'(x) = b_2 + P_2(x)$$

$$\frac{d}{dx} P_3(x) = b_2 + P_2(x)$$

$$\frac{d}{dt} P_3(1-t) = -P_3'(1-t) = b_2 + P_2(1-t)$$

$$b_2 + P_2(x) \text{ is sym about } \frac{1}{2}$$

$$\therefore \frac{d}{dx} P_3(x) = \text{sym}$$

$$\therefore P_3(x) = \text{sym} + \text{const.}$$

$$\text{so } P_3(1-x) = P_3(x) + \text{const}$$

# Proof sketch.

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## STIRLING'S ASYMPTOTIC SERIES.

Gauss used the definition of  $\ln z!$ , valid for any  $z$  with real part  $> -1$ ,

$$z! = \lim_{n \rightarrow \infty} \frac{n! n^z}{(z+1)(z+2)\dots(z+n)} \quad (1)$$

Let  $L(z) = \ln(z!)$ . Then

$$L(z) = \lim [ \ln(n!) + z \ln(n) - \sum_{r=1}^n \ln(z+r) ] \quad (2)$$

$$\text{Differentiate. } L'(z) = \lim [ \ln(n) - \sum_{r=1}^n 1/(z+r) ] \quad (3)$$

$$\begin{aligned} \text{Differentiate } L''(z) &= \lim \sum_{r=1}^n 1/(z+r)^2 \\ &= \sum_{r=1}^{\infty} 1/(z+r)^2 \end{aligned} \quad (4)$$


---

$$\text{Now } \int_0^{\infty} (z+x)^{-2} dx = [-1/(z+x)]_{x=0}^{\infty} = 1/z \quad (5)$$

Euler-Maclaurin gives for any analytic function  $f(x)$

$$\begin{aligned} \int_0^n f(x) dx &= f(0)/2 + f(1) + f(2) + \dots + f(n-1) + f(n)/2 - \\ &\quad - b_2[f'(n) - f'(0)] - b_4[f''(n) - f''(0)] - \dots - \\ &\quad - b_{2r}[f^{(2r-1)}(n) - f^{(2r-1)}(0)] - \\ &\quad - \sum_{m=0}^{n-1} \int_m^{m+1} P_{2r+1}(x-m) f^{(2r+1)}(x) dx \end{aligned} \quad (6)$$

← *dag*

Here  $b_n = B_n/n!$ .

We now take  $f(x) = (z+x)^{-2}$  and let  $n \rightarrow \infty$ , so the integral in (6) makes the left-hand side of (6) equal to  $1/z$ .

Then  $f'(x) = -2(x+z)^{-3}$ ,  $f''(x) = -2 \cdot 3 \cdot 4 (x+z)^{-5}$  and so on. The factorials that appear cause  $b_n$  to be replaced by  $B_n$ . Also all the derivatives tend to zero as  $n \rightarrow \infty$ . Only those involving  $x=0$  survive, and these give negative powers of  $z$ . Thus equation (6) gives

### TENSOR CALCULUS.

Tensor calculus is concerned with objects that are specified in many different systems. As an analogy, suppose our information about a building is based on a number of photographs taken from various viewpoints. All the photographs are different but they all cause us to imagine the same building.

Usually we are concerned with geometrical or physical objects. Suppose an origin has been chosen on a sheet of paper and another point marked. With one choice of axes it may be recorded as (5,0), with another it may be (4,3). We can find the transformation needed to change from one system to the other. We call (a,b) in the first system the same vector as (c,d) in the second if they correspond under the appropriate transformation. The vector is regarded as an objective thing described in many different ways in different systems. The transformations that convert one system to another are always supposed known.

We can express by a formal test what we mean by saying a vector is "an objective thing". We shall regard  $\mathbf{v}$  as a vector if (i) it is specified in each system by a row of numbers, (ii) the numbers in any pair of systems are related by the transformation appropriate to these systems.

We shall be concerned with objects other than vectors. In each case, something is accepted as a tensor if all the users of different systems can agree on what it is. Again the condition for this will be that suitable transformations will enable us to change from one system to another.

Tensors play a great part in general relativity, the basic idea of which is that, among the representations considered, none is to have a privileged position. Different equations will of course appear in different representations, but these must differ only because of the different co-ordinate framework they use; in real terms they must all be saying the same thing.

General relativity accepts the use of curvilinear co-ordinate systems. We shall not consider these here, but restrict our work to linear systems, which are sufficient for special relativity.

Vectors are a particular example of tensors; they have objective meanings, as, for example, displacement, velocity, acceleration. They are known as tensors of order 1.

Tensors of order zero are the simplest of all. They are single numbers that can be transferred from one system to another without any change, and are known as scalars. In Newtonian mechanics mass is a scalar. It does not matter in what directions you choose your axes, masses remain the same.

#### Covariant and contravariant.

With oblique axes, there are two ways of specifying a vector. In (i) we resolve OP into components parallel to the axes. Then OP is recorded as  $x^{(1)}, x^{(2)}$ . Here 1 and 2 label components; they have nothing to do with powers.

In (ii) we drop perpendiculars. OF is then recorded as  $F_1, F_2$ .

Now let  $\begin{pmatrix} 1 & \cos A \\ 0 & 1 \end{pmatrix} = \begin{pmatrix} g_{11} & g_{12} \\ g_{21} & g_{22} \end{pmatrix}$  and  $\begin{pmatrix} 1 & -\sin A \\ 0 & 1 \end{pmatrix} = \begin{pmatrix} g_{11} & g_{12} \\ g_{21} & g_{22} \end{pmatrix}$

Then  $x_1 = g_{11}x^{(1)} + g_{12}x^{(2)}$   
 $x_2 = g_{21}x^{(1)} + g_{22}x^{(2)}$ .

This means  $x_i = g_{ij}x^j$  ... (1)

Now  $OP^2 = \underline{x} \cdot \underline{x} = x^i x_i = x^i g_{ij} x^j = g_{ij} x^i x^j$  ... (2)

Many treatments start from equation (2); it is supposed that the length of every vector is defined and that  $g_{ij}$  are the coefficients that occur in the expression for the square of the length. It is understood that  $g_{ii} = g_{ii}$ .

Equations (1) and (2) are used for work in any (finite) number of dimensions.

We were led to these equations by considering the particular case of 2 dimensions. The theory for n dimensions starts by assuming that length is defined by equation (2). It is then shown that this definition implies the existence of a scalar product, and that equation (1) fits nicely into this. This will be shown in the following section.

### The Polar Form.

Consider any two vectors  $\underline{x}$  and  $\underline{y}$ . Let  $|\underline{x}|$  and  $|\underline{y}|$  denote their lengths. We have

$$\begin{aligned} |\underline{x} + \underline{y}|^2 &= g_{ij}(x^i + y^i)(x^j + y^j) \\ &= g_{ij}x^i x^j + g_{ij}y^i x^j + g_{ij}x^i y^j + g_{ij}y^i y^j \\ &= |\underline{x}|^2 + 2g_{ij}x^i y^j + |\underline{y}|^2 \text{ as } g_{ij} \text{ is symmetric.} \end{aligned}$$

Therefore  $2g_{ij}x^i y^j = |\underline{x} + \underline{y}|^2 - |\underline{x}|^2 - |\underline{y}|^2$ , so  $g_{ij}x^i y^j$  is invariant, i.e. it is a scalar, the same in every system; it is in fact the scalar product of  $\underline{x}$  and  $\underline{y}$ .

We can write the abbreviation  $y_i$  for  $g_{ij}y^j$ , so the scalar product appears in the form  $x^i y_i$ , which we met earlier.

Equation (1) may be regarded as defining  $y_i$ , a symbol that has not been used previously in the general case.

To show that there exists a tridiagonal matrix  $T_3$   
 that commutes with  $H$ , where  $H_{rs} = 1/(r+s+1)$ ,  
 $r, s$  from 0 to  $n$ .

Let  $M$  be the matrix  
 $M$  and  $H$  commute  
 $\Leftrightarrow MH$  is symmetrical.

$$\begin{pmatrix} b_0 & a_0 & 0 & \cdots & 0 \\ a_0 & b_1 & a_1 & \cdots & 0 \\ 0 & a_1 & b_2 & a_2 & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \cdots & a_{n-1} & b_n \end{pmatrix}$$

$$(MH)_{ik} = \sum M_{ij} H_{jk}$$

$$= M_{i,i-1} H_{i-1,k} + M_{i,i} H_{i,k} + M_{i,i+1} H_{i+1,k} \\ = \frac{a_{i-1}}{i+k} + \frac{b_i}{i+k+1} + \frac{a_i}{i+k+2}.$$

This is to equal  $\frac{a_{k-1}}{i+k} + \frac{b_k}{i+k+1} + \frac{a_k}{i+k+2}$ .

If it is understood that  $a_{-1}=0$  and  $a_n=0$ . We require

$$\frac{a_{i-1}-a_{k-1}}{i+k} + \frac{b_i-b_k}{i+k+1} + \frac{a_i-a_k}{i+k+2} = 0 \quad (1)$$

Let  $\varphi(i) = a_{i-1}$ .  $\varphi(i)-\varphi(k)$  automatically has  $i-k$  as a factor. It will have  $i+k$  as a factor (to cancel) if  $\varphi(i)-\varphi(-i)=0$ , the remainder theorem with  $k$  as variable.

Thus we choose an even polynomial for  $\varphi$ .

Try  $a_{i-1} = \alpha i^4 + \beta i^2 + \gamma$ .  $a_{-1}=0$  means  $\gamma=0$ .

$a_n=0$  means  $\alpha(n+1)^4 + \beta(n+1)^2 = 0$  Take  $\alpha=1, \beta=-1/(n+1)^2$

$$a_{i-1} = i^4 - (n+1)^2 i^2, \quad a_i = (i+1)^4 - (n+1)^2 (i+1)^2$$

This automatically gives cancelling in  $(a_i-a_k)/(i+k+2)$ , since this comes from  $(a_{i-1}-a_{k-1})/(i+k)$  by  $i \rightarrow i+1, k \rightarrow k+1$ .

We would like  $b_i-b_k$  to have the factor  $i+k+1$ .

Let  $b_i = 4(i) - 4(k)$   $\psi(i) - \psi(k)$  is zero for  $i = -k-1$  if  $\psi(-k-1) - \psi(k) = 0$  This will happen if  $\psi(k)$  is an even function of  $k+\frac{1}{2}$ .

$$Let b_k = p(k+\frac{1}{2})^4 + q(k+\frac{1}{2})^2$$

(2)

T4

A routine calculation gives

$$\frac{a_{i+1} - a_{k-1}}{i+k} = \frac{a_i - a_k}{i+k-2} = (i-k) [2i^2 + 2k^2 + 2i + 2k + 2 - 2(n+1)^2]$$

$$\frac{b_i - b_k}{i+k-1} = (i-k) [P(i^2 + k^2 + i + k + \frac{1}{2}) + q]$$

all terms in eqn. 1

The terms involving  $i, k$  in the sum of these will disappear if  $P = -2$ . There will remain

$$q + 1 - 2(n+1)^2 \text{ which will be zero}$$

$$q = 2n^2 + 4n + 1.$$

$$\text{Thus } a_i = (i+1)^4 - (n+1)^2(i+1)^2$$

$$b_i = -2(i + \frac{1}{2})^4 + (2n^2 + 4n + 1)(i + \frac{1}{2})^2$$

gives a tridiagonal matrix,  $n+1$  by  $n+1$ , commuting with the Hilbert matrix with  $n+1$  rows and columns.

T5

$$\frac{a_{i-1} - a_{i+k}}{i+k} + \frac{b_i - b_{i+k}}{i+k+1} + \frac{a_i - a_{i+k}}{i+k+2} = 0$$

We want  $b_i - b_{i+k}$  to have factor  $i+k+1$

$$\therefore b(-k-1) = b(k)$$

$$\text{If } u = k + \frac{1}{2} \quad \begin{array}{l} k = u - \frac{1}{2} \\ -k = -u + \frac{1}{2} \end{array}$$

$$\text{Let } -k = u + \alpha \quad -k-1 = -u - \alpha - 1$$

$$b(u + \alpha) = b(-u - \alpha - 1)$$

$$\text{If } \alpha = -\frac{1}{2} \quad \begin{array}{c} -k-1 \\ b(u - \frac{1}{2}) = b(-u - \frac{1}{2}) \end{array} \quad \begin{array}{c} -k-1 \\ \vdots \\ k \end{array}$$

i.e.  $b(u - \frac{1}{2})$  is unchanged by  $u \rightarrow -u$

i.e.  $b(u - \frac{1}{2})$  is even of  $u$ .

$$b(k) \quad \begin{array}{c} \dots \\ k + \frac{1}{2} \end{array}$$

$$\text{Let } b(k) = p(k + \frac{1}{2})^k + q(k - \frac{1}{2})^k$$

$$\frac{b(i) - b(k)}{i+k+1} = \frac{p[(i + \frac{1}{2})^k - (k + \frac{1}{2})^k] + q[(i - \frac{1}{2})^k - (k - \frac{1}{2})^k]}{i+k+1}$$

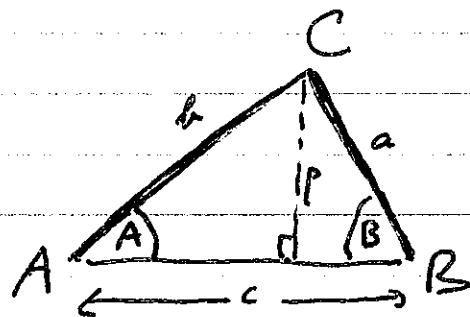
$$= \frac{p[(i + \frac{1}{2})^k - (k + \frac{1}{2})^k]}{i+k+1} [(i + \frac{1}{2})^k + (k + \frac{1}{2})^k] + q(i+k+1)(i-k)$$

$$= p(i-k)[(i + \frac{1}{2})^k + (k + \frac{1}{2})^k] + q(i-k)$$

$$= p(i-k)(i^2 + k^2 + i + k + \frac{1}{2}) + q(i-k)$$

T<sub>6</sub>

## Trigonometry of General Triangle



$$\sin A = \frac{p}{b}$$

$$p = b \sin A.$$

$$p = b \sin A$$

$$p = a \sin B$$

$$\therefore b \sin A = a \sin B$$

÷ ab

$$\frac{\sin A}{a} = \frac{\sin B}{b}$$

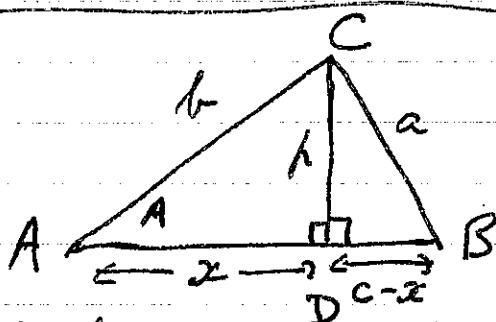
$$= \frac{\sin C}{c} \quad \text{by symmetry}$$

Sine Rule.

Cosine Rule -

Two eqns required, as

There are two unknowns p, x.



Pythagoras for  $\triangle ADC$ :  $x^2 + p^2 = b^2$

---  $\triangle BCP$ :  $(c-x)^2 + p^2 = a^2$

We can get an eqn. involving x alone.

$$(2) - (1): (c-x)^2 - x^2 = a^2 - b^2$$

$$(c^2 + x^2 - 2cx) - x^2 = a^2 - b^2$$

$$c^2 - 2cx = a^2 - b^2$$

Solve for x.  $c^2 = a^2 + b^2 + 2cx$

Add  $-a^2 + b^2$

$$c^2 - a^2 + b^2 = 2cx$$

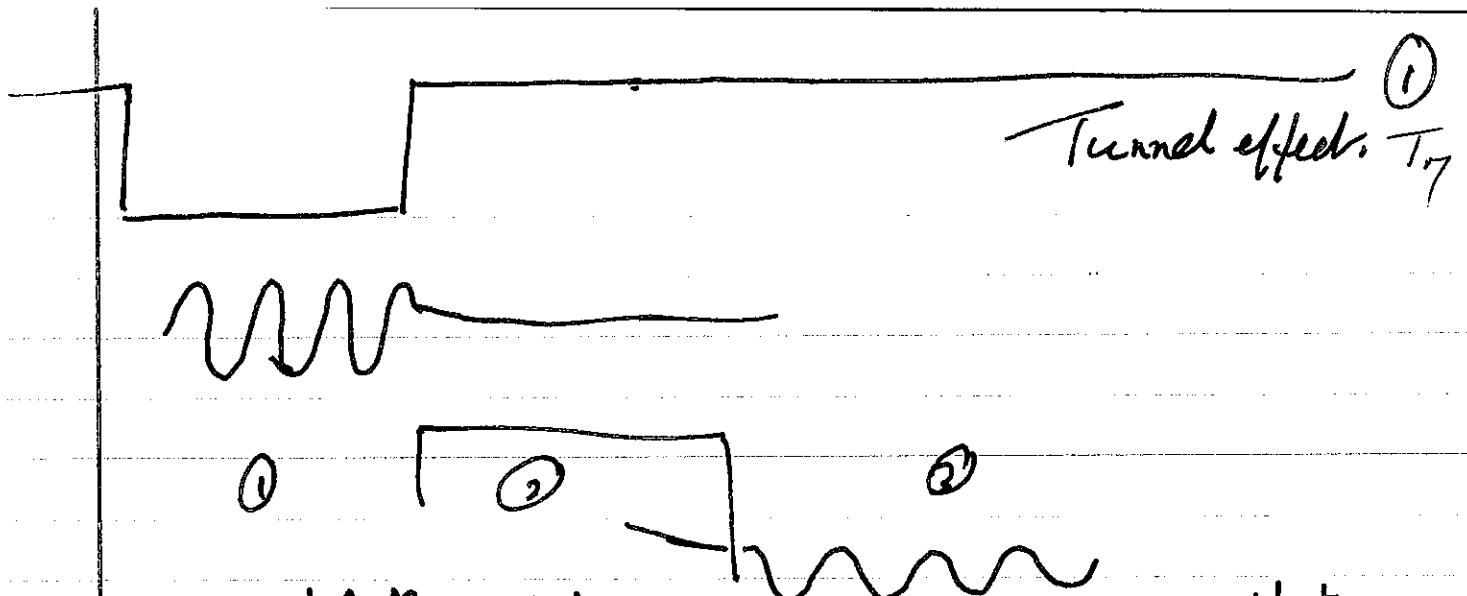
$$\div 2c$$

$$x = \frac{c^2 + b^2 - a^2}{2c}$$

$$\cos A = \frac{c^2}{b^2}$$

$$\therefore \cos A = \frac{b^2 + c^2 - a^2}{2bc}$$

Note symmetry  
a coupled at  
b, c enter in the  
same way.



What worried me in this discussion was that we have an real exponential  $B e^{-x}$  and in ②.  $\psi, \psi'$  both real at junction of ② and ③ so a real sine wave would just onto them.

$$\text{But if } \psi = P \sin(\omega x + \epsilon)$$

$|\psi|^2$ , the probability, has maxima and minima.

which it should not have  $|Ke^{i\mu x}|$  is the accepted wave function for electron moving freely  $|\psi|^2 = K^2$  constant.

For an electron trapped in an interval,  $\psi = \sin x$  is accepted. see e.g. Yarwood, Atomic & Nuclear Physics § 6.11.

What I had overlooked in the brief argument above is that we can eliminate the term  $e^x$  in region ②, if it extends to infinity

$$Ae^x + Be^{-x}$$

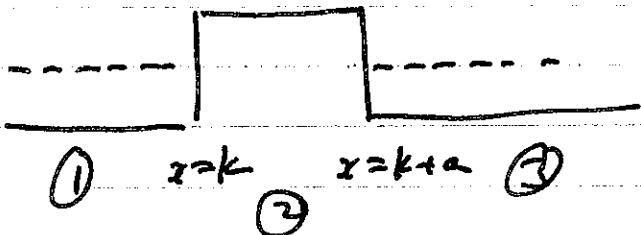
$A=0$  if ② extends indefinitely.

No need to assume  $A=0$ , if barrier terminates. Our only misgiving is — will not  $e^x$  give much too large a wave energy?

(2)

T<sub>8</sub>

Fresh treatment of limited barrier.



$$\psi'' + \psi = 0 \text{ in } ①$$

$$\psi'' - \psi = 0 \text{ in } ②$$

$$\psi'' + \psi = 0 \text{ in } ③$$

$$\text{We suppose } \psi = cx^2 \text{ in } ①$$

$$\psi = Ae^{kx} + Be^{-kx} \text{ in } ②$$

$$\psi = Ce^{ix} \text{ in } ③$$

Continuity of  $\psi$  and  $\psi'$ 

$$(i) \cos k = Ae^k + Be^{-k} \quad (ii) Ae^{k+a} + Be^{-k-a} = Ce^{i(k+a)}$$

$$(iii) -\sin k = Ae^k - Be^{-k} \quad (iv) Ae^{k+a} - Be^{-k-a} = iCe^{i(k+a)}$$

$$\text{From (i) and (ii)} \quad A e^k = \frac{1}{2}(\cos k - \sin k) \quad B e^{-k} = \frac{1}{2}(\cos k + \sin k)$$

From (iii) and (iv), eliminating C,

$$Ae^{k+a} - Be^{-k-a} = \left[ \left( Ae^{k+a} + Be^{-k-a} \right) \right]$$

$$Ae^{k+a}(1-i) = Be^{-k-a}(1+i)$$

satisfied if  $Ae^{k+a} = \rho(1+i)$   $B = \rho(1-i)$ 

Substitute in (i)

$$\cos k = \rho e^{-a}(1+i) + \rho e^a(1-i)$$

$$\therefore \rho = \frac{\cos k}{e^{-a}(1+i) + e^a(1-i)}$$

$$\therefore A = \frac{(1+i)e^{-k-a} \cos k}{e^{-a}(1+i) + e^a(1-i)} \quad B = \frac{(1-i)e^{k+a} \cos k}{e^{-a}(1+i) + e^a(1-i)}$$

$$(iii) \rightarrow C = (Ae^{k+a} + Be^{-k-a}) e^{-i(k+a)} \\ = [\rho(1+i) + \rho(1-i)] e^{-i(k+a)} = 2\rho e^{-i(k+a)}$$

$$\therefore C = \frac{2 \cos k e^{-i(k+a)}}{e^{-a}(1+i) + e^a(1-i)}$$

 $e^a$  may be large, but occurs only in denominator.At  $(e^{-i(k+a)}) = 1$  the exponential due not matter here.

(3)

$$\psi = Ce^{ix} \quad \Psi = Ce^{ix} e^{-iEt/\hbar}$$

T9

In wave mechanics, the classical quantities are replaced by operators. If  $O\hat{\tau}$  is some operator representing a quantity, a situation in which  $O\hat{\tau}$  has the definite value  $a$  will have  $O\hat{\tau}\Psi = a\Psi$ , i.e.  $\Psi$  is an eigenfunction for  $O\hat{\tau}$ .

For example, energy has the operator  $i\hbar \frac{\partial}{\partial t}$ . An electron moving freely has a definite energy, for  $i\hbar \frac{d\Psi}{dt} = i\hbar \left[ -\frac{iE}{\hbar} C e^{ix} e^{-iEt/\hbar} \right]$

$$= E C e^{ix} e^{-iEt/\hbar} = E\Psi.$$

Momentum,  $p_x$ , is given by  $-i\hbar \frac{\partial}{\partial x}$ . This also has  $\Psi$  as an eigenfunction

$$-i\hbar \frac{\partial\Psi}{\partial x} = -i\hbar \cdot i C e^{ix} e^{-iEt/\hbar} = \hbar \Psi$$

so  $p_x$  has the definite value  $\hbar$ .

$$E = \frac{1}{2} M \dot{x}^2 = \hbar \ddot{x} = M \ddot{x} \text{ so } E = \frac{1}{2} \frac{\hbar^2}{M}$$

$$E = \frac{\hbar^2}{2M} = \frac{\hbar^2}{8\pi^2 M} \quad \frac{\hbar}{2\pi}$$

We chose energy at the outset to make

$$(E-V) \frac{8\pi^2 M}{\hbar^2} = 1 \text{ at } V=0, \quad E = \frac{\hbar^2}{8\pi^2 M}$$

in agreement with the above.

④  
 $T_{10}$

In finding  $p_x$  we can neglect time factor, for  $\frac{\partial}{\partial t}$  leaves it unchanged.

$\psi_+ = e^{dix}$  and  $\psi_- = e^{-dix}$  are interesting.

$$-it \frac{\partial^2}{\partial x^2} \psi_+ = -it \cdot dix e^{dix} = dt e^{dix} = dt \psi_+$$

So this represents a particle with  $p_x = dt$

$$-it \frac{\partial^2}{\partial x^2} \psi_- = -it (-dix e^{-dix}) = -tde^{-dix}$$

So  $\psi_-$  has momentum  $-dt$ .

This  $\psi_+$  represents motion to right and  $\psi_-$  to the left.

It is reasonable that only  $\psi_+$  appears in region ③, for electrons emerging from barrier.

In region ① we may have  $\psi = \cos x$ .

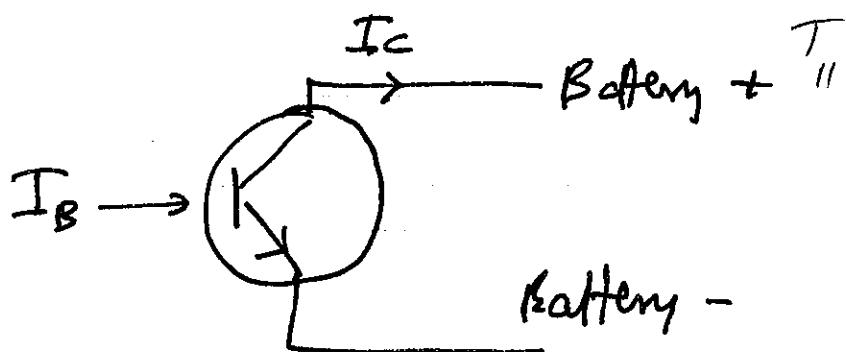
$$\psi = \frac{1}{2}(e^{ix} + e^{-ix})$$

superposition of wave to right and to left.

Transistor.

$I_B$  Base current

$I_c$  Collector current.



NPN Transistor.

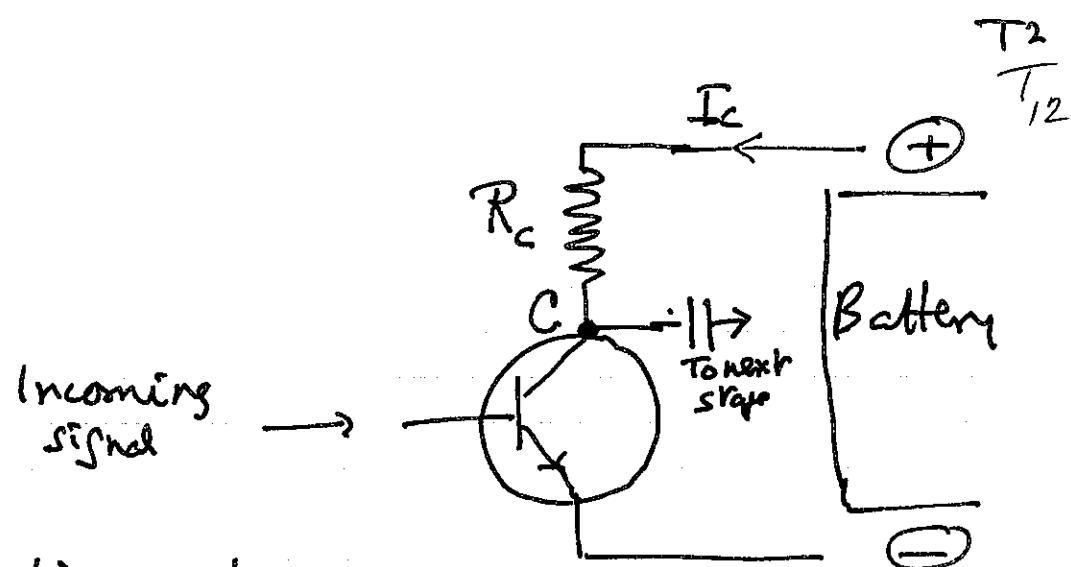
To design a Transistor radio, a fair amount of knowledge is required. However, an understanding of how a transistor behaves requires only a simple picture of what is happening.

If we turn a tap on a hose, a small turn of the tap may produce a large increase in the pressure of the emerging jet. In a transistor, the current going into the base plays a role similar to that of the tap. A change in  $I_B$  produces a much larger change in  $I_c$ . The energy of course is provided by the battery. The base current controls the rate at which this energy is released.

I obtained the following rough values with rather crude apparatus.

$I_B$ (microamps)	$I_c$ (microamps)
10	40
20	100
30	190
40	300
50	400
60	550
70	700
80	850
90	950

It will be seen that, for  $I_B \geq 30$ , an increase of  $10 \mu A$  in  $I_B$  produces a change between  $100 \mu A$  and  $150 \mu A$  in  $I_c$ . The divisions on the scales were too few to permit accurate readings. The effect however is clear.



In the diagram above, the collector  $C$  was connected directly to the battery. However, in a radio receiver this is not so. If  $C$  is connected to the battery directly, its voltage will remain constant. It will not be possible to pass on to the next stage of the receiver information about the changing current  $I_c$ . Accordingly, we always have a resistor,  $R_C$ , between  $C$  and the battery. The current,  $I_c$ , will produce a voltage drop,  $R_C I_c$ , between the ends of this resistor. If the battery has the constant voltage,  $E$ , the collector voltage,  $V_C$  is given by

$$V_C = E - R_C I_c.$$

This is shown in the following experimental results

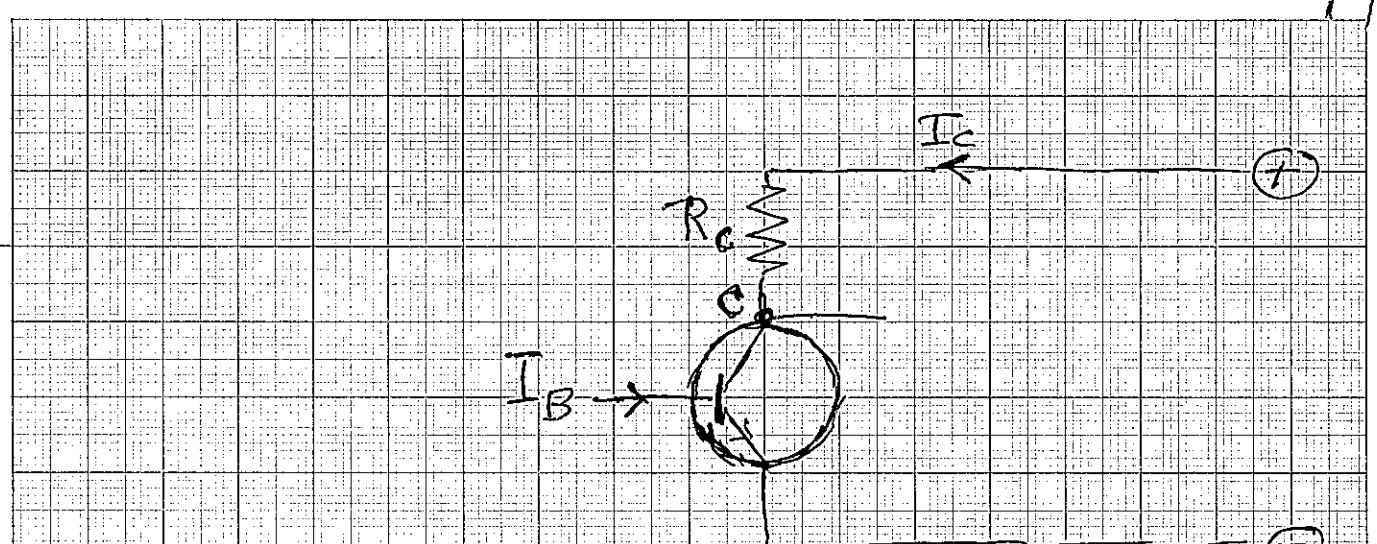
$I_B$	$I_C$ (mA)	$V_C$
4	0.45	3.93
6	0.73	2.02
8	1.05	0.3
10	1.15	0.155
15	1.15	0.113
20	1.18	0.103

The effect of the falling  $V_C$  is that the current  $I_c$  fails to rise even for quite large increases in  $I_B$ .

\* Microammeter with shunt. Microamps are about 12 times the numbers shown here.

The readings are far from accurate, but show the general effect.

T 13



$V_C$

4  
3.9

$I_C$

1.2  
1.1  
1.0  
0.9  
0.8  
0.7  
0.6  
0.5  
0.4  
0.3  
0.2  
0.1

$I_C$

-2

Chartwell

A4 210 x 297 mm

$\rightarrow I_B$

0.3  
0.2  
0.1

250

66

T  
14

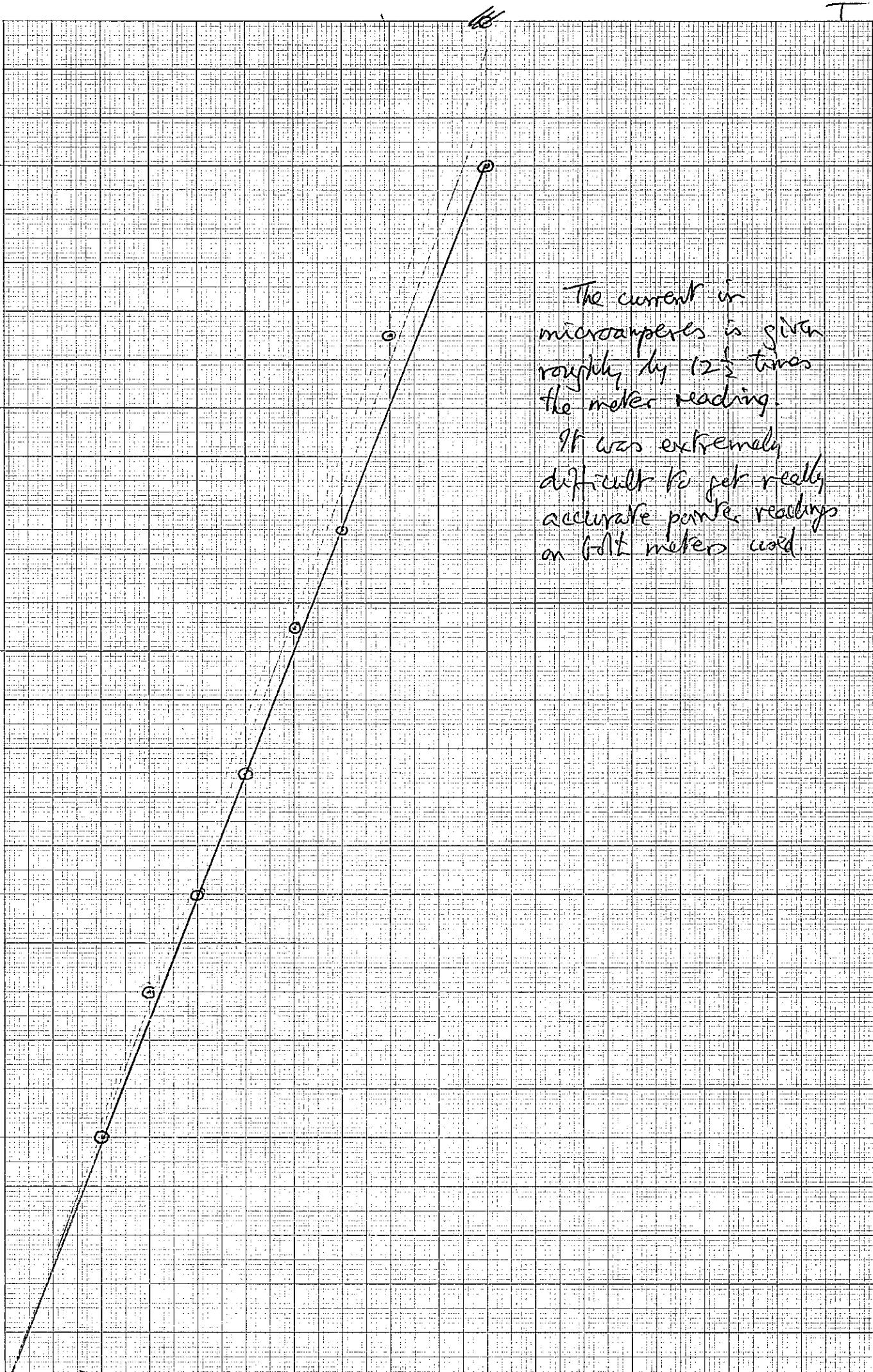
250

200

150

100

50

 $\mu A$   
↑

The current in microamperes is given roughly by 12½ times the meter reading.

It was extremely difficult to get really accurate percentage readings on both meters used.

## H.C. Hall: Applied Electricity

p180. Purely inductive circuit.

$$\text{voltage } v = E \sin \omega t = L \frac{di}{dt} \quad \text{--- (1)}$$

$$\therefore i = -\frac{E}{\omega L} \cos \omega t = \frac{E}{\omega L} \sin(\omega t - \frac{\pi}{2}) \quad \text{--- (1)}$$

A purely inductive circuit does not dissipate any power.

Current lags behind voltage by  $90^\circ$ .

p182 Purely capacitive circuit.  $\frac{1}{C}$ 

$$v = \frac{q}{C} = E \sin \omega t$$

$$q = EC \sin \omega t \quad \left. \begin{array}{l} \\ \end{array} \right\} \quad \text{--- (2)}$$

$$i = \frac{dq}{dt} = EC \omega \cos \omega t \\ = EC \omega \sin(\omega t + \frac{\pi}{2})$$

Current leads voltage by  $90^\circ$ .

At time  $t + \frac{\pi}{2\omega}$ , (1) shows  $v = E \sin(\omega t + \frac{\pi}{2})$ 

$$i = \frac{E}{\omega L} \sin \omega t$$

~~If~~ if  $i = i_0 \sin \omega t$ ,  $E = \frac{\omega L i}{\sin \omega t} = \omega L i_0$

$$\text{and } v = \omega L i_0 \sin(\omega t + \frac{\pi}{2}) ?$$

$$\text{When } i = i_0 \sin \omega t$$

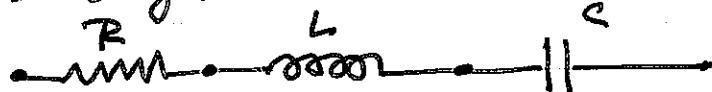
In (2), at time  $t - \frac{\pi}{2\omega}$   $v = E \sin(\omega t - \frac{\pi}{2})$ 

$$i = EC \omega \sin \omega t.$$

$$\text{If } i = i_0 \sin \omega t \quad EC \omega = i_0 \quad E = i_0 / \omega$$

$$v = \frac{i_0}{\omega C} \sin(\omega t - \frac{\pi}{2})$$

If a circuit contains resistance, inductance and capacity, we can think of these as being in series. In fact, resistance is distributed in the inductance coil, but the series picture seems to give correct results.



The same current flows through R and L and into C. Call it  $i_0 \sin \omega t$ . Then the voltage drops are summed in

$$R i_0 \sin \omega t + \omega L i_0 \sin(\omega t + \frac{\pi}{2}) + \frac{i_0}{\omega C} \sin(\omega t - \frac{\pi}{2}) \\ = 9 \left[ R i_0 e^{j\omega t} + \omega L i_0 e^{j\omega t + \frac{\pi}{2}} + \frac{i_0}{\omega C} e^{j\omega t - \frac{\pi}{2}} \right]$$

$$\text{Now } e^{j\pi/2} = (\cos + j \sin) \frac{\pi}{2} = j.$$

$$e^{-j\pi/2} = j = -j.$$

Thus voltage drop across circuit is

$$9 \left[ R i_0 e^{j\omega t} + \omega L j e^{j\omega t} - \frac{i_0}{\omega C} e^{j\omega t} \right] \\ = 9 \left[ \left( R + \omega L j + \frac{-1}{\omega C j} \right) i_0 e^{j\omega t} \right]$$

As  $i_0 e^{j\omega t}$  is the current, this looks like Ohm's Law, since  $\text{voltage} = R \times \text{current}$ .

Using the 9( ) convention, we can work just as if the inductance had resistance  $\omega L j$  and the capacitor  $\frac{1}{\omega C j}$ .

The term impedance is used for this generalized resistance

The flow of currents in a network is determined by Kirchhoff's two laws.

(1) Ohm's Law. A current  $i$  amps can flow through a resistance  $R$  only if there is a voltage difference  $Ri$  between the ends of the resistance.

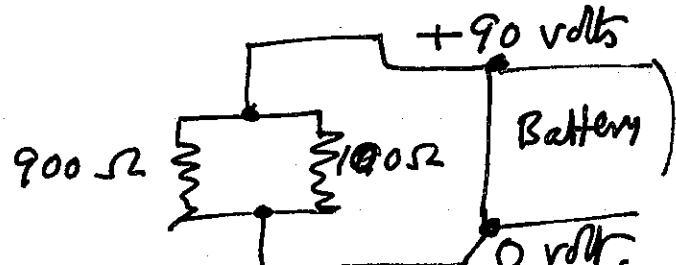
(2) As much current flows out of a junction as flows into it.

Given these two principles, algebra will decide what happens.

Problem 1.

What current flows in each resistor?

What current does the battery supply?

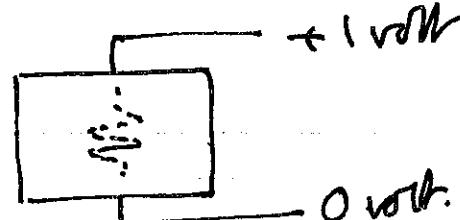
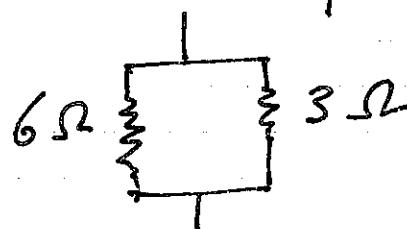


Problem 2

A box is believed to contain a single resistor.

1 volt is applied to its terminals and the current that flows is measured.

On opening the box it is found to contain



What single resistor did they calculate was in the box?

Problem 3 A sensitive microammeter must not carry a current exceeding 50 microamperes. Its resistance is 950 ohms. What shunt must be put across it, if it is to be used for currents up to 1 milliampere?

## Chap 1. §2. Computable functions and partially computable functions

To do calculations we must have signs for numbers. 18  
 $s_i = 1$ . The number  $n$  is shown as  $\overbrace{1 \dots 1}^n$

$$s_i^n = \underbrace{s_i s_i \dots s_i}_n$$

Def 2.1 With  $n$  we associate tape expression  $\bar{n} = 1^{n+1}$

Def 2.2 With  $(n_1 \ n_2 \ \dots \ n_k)$  we associate tape expression  $\bar{(n_1 \ n_2 \ \dots \ n_k)} = \bar{n_1} B \bar{n_2} B \dots B \bar{n_k}$

Example  $(\bar{2} \bar{3} \bar{0}) = 111 B 1111 B 1$  (occurs  $\nu M$ )

Def 2.3 For any expression  $\langle M \rangle$  = number of times  $\langle P \rangle$  occurs in  $M$ .

Note  $\langle \bar{m} \rangle = m$   $\langle PQ \rangle = \langle P \rangle + \langle Q \rangle$

Def. 2.4  $Z$  a Turing machine for each  $n$  we associate  $\psi_z^{(n)}(x_1 \ x_2 \ \dots \ x_n)$  as follows:-

(1) If  $\exists$  a computation  $Z, x_1 \ \dots \ x_p$  we put

$$\psi_z^{(n)}(m_1 \ m_2 \ \dots \ m_n) = \langle x_p \rangle = \langle \text{Res}_Z(x_1) \rangle$$

(2) otherwise undefined.

Example  $Z$  finds  $m_1 + m_2$ .

$$Z = \begin{array}{l} q_1 1 B q_1 \\ q_1 B R q_2 \\ q_2 1 R q_2 \\ q_2 B R q_3 \\ q_3 1 B q_3 \end{array} \quad \begin{array}{l} \alpha_1 = q_1 1^m B 1^m \\ \rightarrow q_1 B 1^m B 1^m \\ \rightarrow B q_2 1^m B 1^m \\ \vdots \dots \dots \vdots \vdots \\ \rightarrow B 1^m q_2 B 1^m \\ \rightarrow B 1^m B q_3 1^m \\ \rightarrow B 1^m B q_3 B 1^m \end{array}$$

terminates because there is no instruction  
 $q_3 B$ !

$$\psi_z^{(2)}(m_1 \ m_2) = \langle B 1^m B q_3 1^m \rangle = m_1 + m_2.$$

Def 2.5  $f(x_1, \dots, x_n)$  is computable if so  
 partially computable if  $\exists Z$  :-

$$f(x_1, \dots, x_n) = \psi_z^{(n)}(x_1, \dots, x_n).$$

If  $f$  is a total function (defined for all ordered  $n$ -tuples), we say  $f$  is computable.

For a fn only partially computable, the machine may go on for ever without finding an answer, or telling us there is none.

Martin Davis Computability & Unsolvability.  
 (McGraw Hill 1958).

(2)  
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Expression. Finite sequence (perhaps  $\infty$ ) of symbols chosen from  
 $q_1, q_2, \dots, q_i, q_j, q_k, q_e$  - LR.

Quadruples Expression

- (1)  $q_i, S_j, S_k, q_e$
- (2)  $q_i, S_j, R, q_e$
- (3)  $q_i, S_j, L, q_e$
- [4]  $q_i, S_j, q_k, q_e$ .

- (1) ~~In state  $q_i$ , seeing  $S_j$ , replace by  $S_k$ , go to state  $q_e$~~   
 (2) go right, state  $q_e$ .  
 (3) go left, state  $q_e$ .

A Turing machine is a set of quadruples, no pair having same pair  $q_i, S_j$  at start. So instruction unambiguous.

{ $q_j$ } internal configurations  
 { $S_j$ } alphabet-

Simple Turing machine uses (1), (2), (3) only.

Symbol  $S_0$  is blank,  $B$ .

In instantaneous description, does not contain  $R$  or  $L$ , contains just one  $q_i$  which is not at extreme right.

Example  $S_0 S_1 q_3 S_2 S_3 S_4$ .

The tape is  $S_0 S_1 S_2 S_3 S_4$ .

The machine is in state  $q_3$ , and looking at  $S_2$ .

Def. An instantaneous description is called terminated if  $\alpha \beta := \alpha \rightarrow \beta$ .

Def. A computation is a sequence of instantaneous descriptions  $\alpha_1 \alpha_2 \dots \alpha_p$  (2) :-  $1 \leq i < p, \alpha_i \rightarrow \alpha_{i+1}$  and  $\alpha_p$  is removed. Then  $\alpha_p = \text{Res}_Z(\alpha_1)$

$\alpha_p$  is the resultant of  $\alpha_1$  wrt  $Z$

(3)  
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Illustration.

$$Z = \left\{ \begin{array}{lll} q_0 S_0 R q_1 & q_1 S_2 R q_1 & q_1 S_5 R q_1 \\ q_1 S_5 S_5 q_2 & q_2 S_8 L q_1 & q_3 S_0 S_5 q_3 \\ q_3 S_2 S_5 q_3 & q_3 S_3 S_5 q_3 & \end{array} \right.$$

If  $\alpha_1 = S_0 q_1 S_0 S_5 S_2$

$$\alpha_1 \rightarrow S_2 S_0 q_1 S_5 S_2$$

$$\rightarrow S_2 S_0 S_5 q_1 S_2$$

$$\rightarrow S_2 S_0 S_5 S_2 q_1 S_0$$

$$\rightarrow S_2 S_0 S_5 S_2 S_0 q_1 S_0$$

$\text{Res}_Z(S_2 q_1 S_0 S_5 S_2)$  undefined.

$S_0$  or B is symbol for blank. The characters are on an infinite strip with blanks extending indefinitely on either sides. With each number  $n$  we associate tape

Def. 2.1 With each number  $n$  we associate expression  $\bar{n} = \overbrace{1 \cdots 1}^n$

Def. 2.2 With k tuple we associate

$$(n_1 n_2 \dots n_k) = \overline{n_1} B \overline{n_2} B \dots B \overline{n_k}$$

Def. 2.3 Output:  $\langle M \rangle$  is no. of times 1 occurs in  $M$ .

$$\text{Then } \langle 11 B S_4 q_2 \rangle = 2 \quad \text{Note } \langle \overline{m-1} \rangle = m.$$

Def. 2.4 Z a Turing machine. For each  $n$ , we associate with Z a function  $\psi^{(n)}(x_1 \dots x_n)$

as follows:- let  $\alpha_i = q_i \langle \overline{m_i} \dots \overline{m_n} \rangle$

$$(1) \text{ If there is a computation of } Z, \quad \alpha_i \dots \alpha_p \quad \psi_Z^{(n)}(\overline{m_1} \dots \overline{m_n}) = \langle \alpha_p \rangle \\ = \langle \text{Res}_Z(\alpha_i) \rangle$$

(2) If no such computation, i.e  $\text{Res}_Z(x_i)$  undefined  $\psi_Z^{(n)}$  is undefined.

$\psi_Z^{(n)}(x)$  written  $\psi_Z(x)$ .

Def. 2.5  $f(x_1, \dots, x_n)$  is called partially computable  
if  $\exists Z$  :-  $f(x_1, \dots, x_n) = \psi_z^{(n)}(x_1, \dots, x_n)$   $\forall z$   
for any  $x_1, \dots, x_n$  in domain of  $f$

Computable if  $f(x_1, \dots, x_n)$  is total function  
(Cdefined for all n-tuples).

Examples follow. If  $f(x_1, y) = x - y$  defined only  
for  $x \geq y$ . Partially computable

§ 4. Relatively computable functions.  
 $T\Gamma^n$  of computability is a special case.

$\mathcal{A}$  is set of numbers

Def. 4.1.  $\alpha \xrightarrow{\mathcal{A}} \beta(z)$ . If  $\alpha = P q_i S_j Q$   
 $Z$  contains  $q_i S_j q_k q_e$

(1) If  $\langle \alpha \rangle \in \mathcal{A}$   $\beta = P q_k S_j Q$

(2) If  $\langle \alpha \rangle \notin \mathcal{A}$ ,  $\beta = P q_e S_j Q$ .

Thus the next operation is carried out  
 $q_k \in \langle \alpha \rangle$  in  $\mathcal{A}$ , to  $q_e$  otherwise.

Def. 4.2  $\alpha = P q_i S_j Q$ .  $\alpha$  is final wrt  $Z$   
if  $Z$  has no ~~initial~~ quadruple

with initial symbols  $q_i S_j$

Theorem 4.1 If  $Z$  is simple, then  $\alpha$  is  
final wrt  $Z$  iff it is final wrt  $Z$

terminal wrt  $Z$  iff it is final wrt  $Z$  iff

Theorem 4.2  $\alpha$  is final wrt  $Z$

(1)  $\alpha$  is terminal wrt  $Z$  iff  $\mathcal{A}$  is closed

(2) No matter what for  $\alpha \xrightarrow{\mathcal{A}} \beta(z)$ .

$\exists \beta := \alpha \xrightarrow{\mathcal{A}} \beta(z)$

Def 4.3 An  $A$ -computation of  $Z$  is  
finite sequence  $\alpha_1, \alpha_2, \dots, \alpha_p :=$  for  $1 \leq i < p$

$\alpha_i \rightarrow \alpha_{i+1}(z) \text{ or } \alpha_i \rightarrow_{dec} \alpha_{i+1}(z)$

and  $\alpha_p$  is final.

Then  $\alpha_p = Res_Z^A(\alpha_1)$  and

$\alpha_p$  is A result of  $\alpha_1$  wrt  $Z$

If  $Z$  is a simple Turing machine, then the definition of  $\psi$ - $\beta$   
is independent of  $A$  and an  $A$  computation in this sense  
is simply a computation in the sense of Def 1.9.

[For  $\xrightarrow{A} \beta(z)$  can never hold if  $Z$  is a simple T  
Turing machine. For, by 4.1.,  $\xrightarrow{A} \beta(z)$  requires  
 $Z$  to contain  $q_1 \xrightarrow{S_1} q_1, q_2$ , which a simple  
machine does not.]

Def 4.4.  $Z$  Turing machine. For each  $n$  we  
associate with  $Z$  a function  $\psi_{Z:A}^{(n)}(x_1, \dots, x_n)$   
[generally depending on  $A$ ], as follows:

For each  $(m_1, \dots, m_n)$  we set  $\alpha_i = q_1(m_1, m_2, \dots, m_n)$

(1) If  $Z$  computation  $f$  an  $A$  computation of  $Z$ ,

$$\alpha_1, \alpha_2, \dots, \alpha_p \psi_{Z:A}^{(n)}(m_1, \dots, m_n) = \langle \alpha_p \rangle = \langle \text{Rec}_Z^A(\alpha_1) \rangle$$

(2) If not,  $\psi$  is undefined.

$\psi_Z^A(x)$  mean  $\psi_{Z:A}^{(1)}(x)$ .

If  $Z$  is simple, by remark above

$$\psi_{Z:A}^{(n)}(x_1, \dots, x_n) = \psi_Z^{(n)}(x_1, \dots, x_n).$$

Def 4.5  $f(x_1, \dots, x_n)$  is partially  $A$ -computable

if  $\exists$  Turing machine  $Z$  :-

$$f(x_1, \dots, x_n) = \psi_{Z:A}^{(n)}(x_1, \dots, x_n)$$

If so we say  $Z$   $A$ -computes  $f$ .

If in addition  $f$  is total fn,  $f$  is  
called  $A$ -computable.